<table>
<thead>
<tr>
<th>S.NO</th>
<th>CONTENTS</th>
<th>PAGE.NO</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td><strong>UNIT–1 FEED BACK AMPLIFIERS</strong></td>
<td>1 to 15</td>
</tr>
<tr>
<td>1.1</td>
<td>Feedback</td>
<td>1</td>
</tr>
<tr>
<td>1.2</td>
<td>Principles of Negative Voltage Feedback In Amplifiers</td>
<td>2</td>
</tr>
<tr>
<td>1.3</td>
<td>1.3 Gain of Negative Voltage Feedback Amplifier</td>
<td>3</td>
</tr>
<tr>
<td>1.4</td>
<td>1.4 Advantages of Negative Voltage Feedback</td>
<td>4</td>
</tr>
<tr>
<td>1.5</td>
<td>Feedback Circuit</td>
<td>6</td>
</tr>
<tr>
<td>1.6</td>
<td>Principles of Negative Current Feedback</td>
<td>6</td>
</tr>
<tr>
<td>1.7</td>
<td>Current Gain with Negative Current Feedback</td>
<td>7</td>
</tr>
<tr>
<td>1.8</td>
<td>Effects of Negative Current Feedback</td>
<td>7</td>
</tr>
<tr>
<td>1.9</td>
<td>Emitter Follower</td>
<td>9</td>
</tr>
<tr>
<td>1.11</td>
<td>D.C. Analysis of Emitter Follower</td>
<td>10</td>
</tr>
<tr>
<td>1.12</td>
<td>Voltage Gain of Emitter Follower</td>
<td>10</td>
</tr>
<tr>
<td>1.13</td>
<td>Input Impedance of Emitter Follower</td>
<td>12</td>
</tr>
<tr>
<td>1.14</td>
<td>Output Impedance of Emitter Follower</td>
<td>13</td>
</tr>
<tr>
<td>1.15</td>
<td>Applications of Emitter Follower</td>
<td>14</td>
</tr>
<tr>
<td></td>
<td>Nyquist Criterion</td>
<td>15</td>
</tr>
</tbody>
</table>

<p>|      | <strong>UNIT–2 OSCILLATORS</strong>                             | 16-34   |
| 2.1  | Introduction about Oscillators                     | 16      |
| 2.2  | Mechanism of start of oscillation                   | 17      |
| 2.3  | Basic Oscillator Feedback Circuit                   | 17      |
| 2.3.1| Without Feedback                                    | 18      |
| 2.3.2| With Feedback                                       | 18      |
| 2.3.3| Resonance                                           | 18      |</p>
<table>
<thead>
<tr>
<th>Section</th>
<th>Title</th>
<th>Page</th>
</tr>
</thead>
<tbody>
<tr>
<td>2.4</td>
<td>Basic LC Oscillator Tank Circuit</td>
<td>19</td>
</tr>
<tr>
<td>2.4.1</td>
<td>Damped Oscillations</td>
<td>20</td>
</tr>
<tr>
<td>2.4.2</td>
<td>Resonance Frequency</td>
<td>20</td>
</tr>
<tr>
<td>2.4.3</td>
<td>Resonant Frequency of a LC Oscillator</td>
<td>21</td>
</tr>
<tr>
<td>2.5</td>
<td>Basic Transistor LC Oscillator Circuit</td>
<td>22</td>
</tr>
<tr>
<td>2.6</td>
<td>The Hartley Oscillator</td>
<td>22</td>
</tr>
<tr>
<td>2.6.1</td>
<td>Hartley Oscillator Tuned Circuit</td>
<td>23</td>
</tr>
<tr>
<td>2.6.2</td>
<td>Basic Hartley Oscillator Circuit</td>
<td>24</td>
</tr>
<tr>
<td>2.6.3</td>
<td>Shunt-fed Hartley Oscillator Circuit</td>
<td>25</td>
</tr>
<tr>
<td>2.7</td>
<td>Armstrong oscillator</td>
<td>25</td>
</tr>
<tr>
<td>2.8</td>
<td>The Colpitts Oscillator</td>
<td>25</td>
</tr>
<tr>
<td>2.9</td>
<td>Colpitts Oscillator Circuit</td>
<td>26</td>
</tr>
<tr>
<td>2.9.1</td>
<td>Basic Colpitts Oscillator Circuit</td>
<td>26</td>
</tr>
<tr>
<td>2.9.2</td>
<td>Colpitts Oscillator using an Op-amp</td>
<td>27</td>
</tr>
<tr>
<td>2.1</td>
<td>RC Phase-Shift Oscillator</td>
<td>28</td>
</tr>
<tr>
<td>2.10.1</td>
<td>Op-amp RC Oscillator Circuit</td>
<td>29</td>
</tr>
<tr>
<td>2.11</td>
<td>WIEN BRIDGE OSCILLATOR</td>
<td>30</td>
</tr>
<tr>
<td>2.12</td>
<td>Quartz Crystal Oscillators</td>
<td>31</td>
</tr>
<tr>
<td>2.13</td>
<td>Pierce Oscillator</td>
<td>34</td>
</tr>
</tbody>
</table>

**UNIT–3**

**TUNED AMPLIFIERS**

<table>
<thead>
<tr>
<th>Section</th>
<th>Title</th>
<th>Page</th>
</tr>
</thead>
<tbody>
<tr>
<td>3.1</td>
<td>Introduction to tuned circuits</td>
<td>35</td>
</tr>
<tr>
<td>3.2</td>
<td>Resonance circuits</td>
<td>35</td>
</tr>
<tr>
<td>3.3</td>
<td>Need for tuned circuits</td>
<td>36</td>
</tr>
<tr>
<td>3.4</td>
<td>Applications of tuned amplifier</td>
<td>36</td>
</tr>
<tr>
<td>3.5</td>
<td>CLASSIFICATION</td>
<td>37</td>
</tr>
<tr>
<td>3.5.1</td>
<td>Single tuned amplifier</td>
<td>37</td>
</tr>
</tbody>
</table>

SCE  
Dept.of ECE
UNIT–4 WAVE SHAPING AND MULTIVIBRATOR CIRCUITS  44 to 61

4.1 RL circuit 44
4.2 The RC Integrator 44
4.3 RL INTEGRATORS 46
4.4 Multivibrators 47
   4.4.1 Astable Multivibrator 47
   4.4.2 Bistable multivibrator 50
4.5 Clippers 53
   4.5.1 Series clipper 53
4.6 Clamper 55
   4.6.1 Positive Clamper 57
   4.6.2 Negative Clamper 58
4.7 Schmitt Trigger 58

UNIT V– BLOCKING OSCILLATORS AND TIMEBASE GENERATORS 62 to 77

5.1 Waveform Generator 62
5.2 Time-Base Generators 62
5.3 Unijunction Sawtooth Generator 63
5.4 UJT Relaxation Oscillator 64
5.5 Pulse Transformer 66
5.6 Blocking Oscillator 66
OBJECTIVES:
The student should be made to
- Learn about biasing of BJTs and MOSFETs
- Design and construct amplifiers
- Construct amplifiers with active loads
- Study high frequency response of all amplifiers

UNIT I  POWER SUPPLIES AND BIASING OF DISCRETE BJT AND MOSFET  9
Rectifiers with filters- DC Load line, operating point, Various biasing methods for BJT-Design-Stability-Bias compensation, Thermal stability, Design of biasing for JFET, Design of biasing for MOSFET

UNIT II  BJT AMPLIFIERS  9

UNIT III  JFET AND MOSFET AMPLIFIERS  9
Small signal analysis of JFET amplifiers- Small signal Analysis of MOSFET and JFET, Common source amplifier, Voltage swing limitations, Small signal analysis of MOSFET and JFET Source follower and Common Gate amplifiers, - BiMOS Cascode amplifier

UNIT IV  FREQUENCY ANALYSIS OF BJT AND MOSFET AMPLIFIERS  9
Low frequency and Miller effect, High frequency analysis of CE and MOSFET CS amplifier, Short circuit current gain, cut off frequency – fα and fβ unity gain and Determination of bandwidth of single stage and multistage amplifiers

UNIT V  IC MOSFET AMPLIFIERS  9
IC Amplifiers- IC biasing Current steering circuit using MOSFET- MOSFET current sources-PMOS and NMOS current sources. Amplifier with active loads - enhancement load, Depletion load and PMOS and NMOS current sources load- CMOS common source and source follower- CMOS differential amplifier- CMRR.

TOTAL (L: 45+T: 15): 60 PERIODS
OUTCOMES:
Upon Completion of the course, the students will be able to:
Design circuits with transistor biasing.
Design simple amplifier circuits.
Analyze the small signal equivalent circuits of transistors.
Design and analyze large signal amplifiers.

TEXT BOOK:

REFERENCES:
UNIT – I

FEED BACK AMPLIFIERS

INTRODUCTION

A practical amplifier has a gain of nearly one million i.e. its output is one million times the input. Consequently, even a casual disturbance at the input will appear in the amplified form in the output. There is a strong tendency in amplifiers to introduce hum due to sudden temperature changes or stray electric and magnetic fields. Therefore, every high gain amplifier tends to give noise along with signal in its output. The noise in the output of an amplifier is undesirable and must be kept to as small a level as possible. The noise level in amplifiers can be reduced considerably by the use of negative feedback i.e. by injecting a fraction of output in phase opposition to the input signal. The object of this chapter is to consider the effects and methods of providing negative feedback in transistor amplifiers.

1.1 Feedback

The process of injecting a fraction of output energy of some device back to the input is known as feedback. The principle of feedback is probably as old as the invention of first machine but it is only some 50 years ago that feedback has come into use in connection with electronic circuits. It has been found very useful in reducing noise in amplifiers and making amplifier operation stable. Depending upon whether the feedback energy aids or opposes the input signal, there are two basic types of feedback in amplifiers viz positive feedback and negative feedback.

(i) Positive feedback. When the feedback energy (voltage or current) is in phase with the input signal and thus aids it, it is called positive feedback. This is illustrated in Fig. 1.1. Both amplifier and feedback network introduce a phase shift of 180°. The result is a 360° phase shift around the loop, causing the feedback voltage $V_f$ to be in phase with the input signal $V_{in}$.

![Figure 1.1](image)

The positive feedback increases the gain of the amplifier. However, it has the disadvantages of increased distortion and instability. Therefore, positive feedback is seldom employed in amplifiers. One important use of positive feedback is in oscillators. As we shall see in the next chapter, if positive feedback is sufficiently large, it leads to oscillations. As a matter of fact, an oscillator is a device that converts d.c. power into a.c. power of any desired frequency.

(ii) Negative feedback. When the feedback energy (voltage or current) is out of phase with the input signal and thus opposes it, it is called negative feedback. This is illustrated in Fig. 1.2. As you can see, the amplifier introduces a phase shift of 180° into the circuit while the feedback network is so designed that it introduces no phase shift (i.e., 0° phase shift). The result is that the feedback voltage $V_f$ is 180° out of phase with the input signal $V_{in}$. 
Negative feedback reduces the gain of the amplifier. However, the advantages of negative feedback are: reduction in distortion, stability in gain, increased bandwidth and improved input and output impedances. It is due to these advantages that negative feedback is frequently employed in amplifiers.

1.2 Principles of Negative Voltage Feedback In Amplifiers

A feedback amplifier has two parts viz an amplifier and a feedback circuit. The feedback circuit usually consists of resistors and returns a fraction of output energy back to the input. Fig. 1.3 *shows the principles of negative voltage feedback in an amplifier. Typical values have been assumed to make the treatment more illustrative. The output of the amplifier is 10 V. The fraction mv of this output i.e. 100 mV is feedback to the input where it is applied in series with the input signal of 101 mV. As the feedback is negative, therefore, only 1 mV appears at the input terminals of the amplifier. Referring to Fig. 1.3, we have, Gain of amplifier without feedback,

\[ A_v = \frac{10 \text{ V}}{1 \text{ mV}} = 10,000 \]

Fraction of output voltage feedback, \( m_v = \frac{100 \text{ mV}}{10 \text{ V}} = 0.01 \)

Gain of amplifier with negative feedback, \( A_{vf} = \frac{10 \text{ V}}{101 \text{ mV}} = 100 \)
The following points are worth noting:

- When negative voltage feedback is applied, the gain of the amplifier is reduced. Thus, the gain of above amplifier without feedback is 10,000 whereas with negative feedback, it is only 100.

- When negative voltage feedback is employed, the voltage actually applied to the amplifier is extremely small. In this case, the signal voltage is 101 mV and the negative feedback is 100 mV so that voltage applied at the input of the amplifier is only 1 mV.

- In a negative voltage feedback circuit, the feedback fraction \( m_v \) is always between 0 and 1.

- The gain with feedback is sometimes called closed-loop gain while the gain without feedback is called open-loop gain. These terms come from the fact that amplifier and feedback circuits form a “loop”. When the loop is “opened” by disconnecting the feedback circuit from the input, the amplifier's gain is \( A_v \), the “open-loop” gain. When the loop is “closed” by connecting the feedback circuit, the gain decreases to \( A_v f \), the “closed-loop” gain.

### 1.3 Gain of Negative Voltage Feedback Amplifier

Consider the negative voltage feedback amplifier shown in Fig. 1.4. The gain of the amplifier without feedback is \( A_v \). Negative feedback is then applied by feeding a fraction \( m_v \) of the output voltage \( e_0 \) back to amplifier input. Therefore, the actual input to the amplifier is the signal voltage \( e_g \) minus feedback voltage \( m_v e_0 \) i.e.,

Actual input to amplifier = \( e_g - m_v e_0 \)

The output \( e_0 \) must be equal to the input voltage \( e_g - m_v e_0 \) multiplied by gain \( A_v \) of the amplifier i.e.,

\[
\frac{e_0}{e_g} = \frac{A_v}{1 + A_v m_v}
\]

![Figure 1.4](image-url)
But $e_0/eg$ is the voltage gain of the amplifier with feedback.

Voltage gain with negative feedback is

$$A_{vf} = \frac{A_v}{1 + A_v m_v}$$

It may be seen that the gain of the amplifier without feedback is $A_v$. However, when negative voltage feedback is applied, the gain is reduced by a factor $1 + A_v m_v$. It may be noted that negative voltage feedback does not affect the current gain of the circuit.

### 1.4 Advantages of Negative Voltage Feedback

The following are the advantages of negative voltage feedback in amplifiers:

**(i) Gain stability.** An important advantage of negative voltage feedback is that the resultant gain of the amplifier can be made independent of transistor parameters or the supply voltage variations.

$$A_{vf} = \frac{A_v}{1 + A_v m_v}$$

For negative voltage feedback in an amplifier to be effective, the designer deliberately makes the product $A_v m_v$ much greater than unity. Therefore, in the above relation, 1 can be neglected as compared to $A_v m_v$ and the expression becomes:

$$A_{vf} = \frac{A_v}{A_v m_v} = \frac{1}{m_v}$$

It may be seen that the gain now depends only upon feedback fraction $m_v$ i.e., on the characteristics of feedback circuit. As feedback circuit is usually a voltage divider (a resistive network), therefore, it is unaffected by changes in temperature, variations in transistor parameters and frequency. Hence, the gain of the amplifier is extremely stable.

**(ii) Reduces non-linear distortion.** A large signal stage has non-linear distortion because its voltage gain changes at various points in the cycle. The negative voltage feedback reduces the nonlinear distortion in large signal amplifiers. It can be proved mathematically that:

$$D_{vf} = \frac{D}{1 + A_v m_v}$$

where  

$D = \text{distortion in amplifier without feedback}$  

$D_{vf} = \text{distortion in amplifier with negative feedback}$

It is clear that by applying negative voltage feedback to an amplifier, distortion is reduced by a factor $1 + A_v m_v$.

**(iii) Improves frequency response.** As feedback is usually obtained through a resistive network, therefore, voltage gain of the amplifier is *independent of signal frequency. The result is that voltage gain of the amplifier will be substantially constant over a wide range of signal frequency. The negative voltage feedback, therefore, improves the frequency response of the amplifier.

**(iv) Increases circuit stability.** The output of an ordinary amplifier is easily changed due to variations in ambient temperature, frequency and signal amplitude. This changes the gain of the amplifier, resulting in distortion. However, by applying negative voltage feedback, voltage gain of the amplifier is stabilised or accurately fixed in value.
This can be easily explained. Suppose the output of a negative voltage feedback amplifier has increased because of temperature change or due to some other reason. This means more negative feedback since feedback is being given from the output. This tends to oppose the increase in amplification and maintains it stable. The same is true should the output voltage decrease. Consequently, the circuit stability is considerably increased.

**(v) Increases input impedance and decreases output impedance.** The negative voltage feedback increases the input impedance and decreases the output impedance of amplifier. Such a change is profitable in practice as the amplifier can then serve the purpose of impedance matching.

**(a) Input impedance.** The increase in input impedance with negative voltage feedback can be explained by referring to Fig. 13.5. Suppose the input impedance of the amplifier is $Z_{in}$ without feedback and $Z_{in}'$ with negative feedback. Let us further assume that input current is $i_1$. Referring to Fig. 13.5, we have,

$$\frac{e_g - m_v e_0}{i_1} = Z_m (1 + A_v m_v)$$

But $e_g/i_1 = Z_{in}'$, the input impedance of the amplifier with negative voltage feedback.

$$Z_{in}' = Z_m (1 + A_v m_v)$$

![Figure 1.5](image)

It is clear that by applying negative voltage feedback, the input impedance of the amplifier is increased by a factor $1 + A_v m_v$. As $A_v m_v$ is much greater than unity, therefore, input impedance is increased considerably. This is an advantage, since the amplifier will now present less of a load to its source circuit.

**(b) Output impedance.** Following similar line, we can show that output impedance with negative voltage feedback is given by:
It is clear that by applying negative feedback, the output impedance of the amplifier is decreased by a factor $1 + Av \, m_v$. This is an added benefit of using negative voltage feedback. With lower value of output impedance, the amplifier is much better suited to drive low impedance loads.

### 1.5 Feedback Circuit

The function of the feedback circuit is to return a fraction of the output voltage to the input of the amplifier. Fig. 13.6 shows the feedback circuit of negative voltage feedback amplifier. It is essentially a potential divider consisting of resistances $R_1$ and $R_2$. The output voltage of the amplifier is fed to this potential divider which gives the feedback voltage to the input. Referring to Fig. 13.6, it is clear that:

\[
\text{Voltage across } R_1 = \left( \frac{R_1}{R_1 + R_2} \right) e_0
\]

\[
\text{Feedback fraction, } m_v = \frac{\text{Voltage across } R_1}{e_0} = \frac{R_1}{R_1 + R_2}
\]

![Figure 1.6](image)

### 1.6 Principles of Negative Current Feedback

In this method, a fraction of output current is feedback to the input of the amplifier. In other words, the feedback current ($I_f$) is proportional to the output current ($I_{out}$) of the amplifier. Fig. 1.7 shows the principles of negative current feedback. This circuit is called current-shunt feedback circuit. A feedback resistor $R_f$ is connected between input and output of the amplifier. This amplifier has a current gain of $A_i$ without feedback. It means that a current $I_1$ at the input terminals of the amplifier will appear as $A_i \, I_1$ in the output circuit i.e., $I_{out} = A_i \, I_1$.

Now a fraction $m_v$ of this output current is feedback to the input through $R_f$. The fact that arrowhead shows the feed current being fed forward is because it is negative feedback.
Note that negative current feedback reduces the input current to the amplifier and hence its current gain.

### 1.7 Current Gain with Negative Current Feedback

Referring to Fig. 13.6, we have,

\[ I_{\text{in}} = I_{1} + I_f = I_{1} + m_i I_{\text{out}} \]

But \( I_{\text{out}} = A_i I_1 \), where \( A_i \) is the current gain of the amplifier without feedback.

\[ I_{\text{in}} = I_{1} + m_i A_i I_1 \]

Current gain with negative current feedback is

\[ A_{if} = \frac{I_{\text{out}}}{I_{\text{in}}} = \frac{A_i I_1}{I_1 + m_i A_i I_1} \]

\[ \text{or} \quad A_{if} = \frac{A_i}{1 + m_i A_i} \]

This equation looks very much like that for the voltage gain of negative voltage feedback amplifier. The only difference is that we are dealing with current gain rather than the voltage gain.

The following points may be noted carefully:

(i) The current gain of the amplifier without feedback is \( A_i \). However, when negative current feedback is applied, the current gain is reduced by a factor \( (1 + m_i A_i) \).

(ii) The feedback fraction (or current attenuation) \( m_i \) has a value between 0 and 1.

(iii) The negative current feedback does not affect the voltage gain of the amplifier.

### 1.8 Effects of Negative Current Feedback

The negative current feedback has the following effects on the performance of amplifiers:

(i) **Decreases the input impedance.** The negative current feedback decreases the input impedance of most amplifiers.

Let

\[ Z_{\text{in}} = \text{Input impedance of the amplifier without feedback} \]
Referring to Fig. 1.8, we have,

$$Z'_{in} = \frac{V_m}{I_1}$$

and

$$Z_{in} = \frac{V_m}{I_m}$$

But

$$V_m = I_1 Z_m$$

and

$$I_m = I_1 + I_f = I_1 + m_i I_{out} = I_1 + m_i A_i I_1$$

Thus the input impedance of the amplifier is decreased by the factor \((1 + m_i A_i)\). Note the primary difference between negative current feedback and negative voltage feedback. Negative current feedback decreases the input impedance of the amplifier while negative voltage feedback increases the input impedance of the amplifier.

**Increases the output impedance.** It can be proved that with negative current feedback, the output impedance of the amplifier is increased by a factor \((1 + m_i A_i)\).

$$Z'_{out} = Z_{out} (1 + m_i A_i)$$

where

\(Z_{out}\) = output impedance of the amplifier without feedback

\(Z'_{out}\) = output impedance of the amplifier with negative current feedback

The reader may recall that with negative voltage feedback, the output impedance of the amplifier is decreased.

**Increases bandwidth.** It can be shown that with negative current feedback, the bandwidth of the amplifier is increased by the factor \((1 + m_i A_i)\).

$$BW' = BW (1 + m_i A_i)$$

where

\(BW\) = Bandwidth of the amplifier without feedback

\(BW'\) = Bandwidth of the amplifier with negative current feedback
1.9 Emitter Follower

It is a negative current feedback circuit. The emitter follower is a current amplifier that has no voltage gain. Its most important characteristic is that it has high input impedance and low output impedance. This makes it an ideal circuit for impedance matching.

Circuit details. Fig. 1.9 shows the circuit of an emitter follower. As you can see, it differs from the circuitry of a conventional CE amplifier by the absence of collector load and emitter bypass capacitor. The emitter resistance $R_E$ itself acts as the load and a.c. output voltage ($V_{out}$) is taken across $R_E$. The biasing is generally provided by voltage-divider method or by base resistor method. The following points are worth noting about the emitter follower:

(i) There is neither collector resistor in the circuit nor there is emitter bypass capacitor. These are the two circuit recognition features of the emitter follower.

(ii) Since the collector is at ac ground, this circuit is also known as common collector (CC) amplifier.

Operation. The input voltage is applied between base and emitter and the resulting a.c. emitter current produces an output voltage $i_ER_E$ across the emitter resistance. This voltage opposes the input voltage, thus providing negative feedback. Clearly, it is a negative current feedback circuit since the voltage feedback is proportional to the emitter current i.e., output current. It is called emitter follower because the output voltage follows the input voltage.

Characteristics.

The major characteristics of the emitter follower are:

(i) No voltage gain. In fact, the voltage gain of an emitter follower is close to 1.

(ii) Relatively high current gain and power gain.

(iii) High input impedance and low output impedance.

(iv) Input and output ac voltages are in phase.
1.10 D.C. Analysis of Emitter Follower

The d.c. analysis of an emitter follower is made in the same way as the voltage divider bias circuit of a CE amplifier. Thus referring to Fig. 1.9 above, we have,

![Image of the emitter follower circuit diagram]

**Figure 1.10**

Voltage across $R_2$, $V_2 = \frac{V_{CC}}{R_1 + R_2} \times R_2$

Emitter current, $I_E = \frac{V_E}{R_E} = \frac{V_2 - V_{BE}}{R_E}$

Collector-emitter voltage, $V_{CE} = V_{CC} - V_E$

**D.C. Load Line.** The d.c. load line of emitter follower can be constructed by locating the two end points viz., $I_{C(sat)}$ and $V_{CE(off)}$.

(i) When the transistor is saturated, $V_{CE} = 0$.

$$I_{C(sat)} = \frac{V_{CC}}{R_E}$$

This locates the point A ($OA = V_{CC}/R_E$) of the d.c. load line as shown in Fig. 1.10.

(ii) When the transistor is cut off, $I_C = 0$. Therefore, $V_{CE(off)} = V_{CC}$. This locates the point B ($OB = V_{CC}$) of the d.c. load line.

By joining points A and B, d.c. load line $AB$ is constructed.

13.11 Voltage Gain of Emitter Follower

Fig. 1.11 shows the emitter follower circuit. Since the emitter resistor is not bypassed by a capacitor, the a.c. equivalent circuit of emitter follower will be as shown in Fig. 1.12. The ac resistance $r_E$ of the emitter circuit is given by

$$r_E = r_E' + R_E \quad \text{where} \quad r_E' = \frac{25 \text{ mV}}{I_E}$$
In order to find the voltage gain of the emitter follower, let us replace the transistor in Fig. 1.12 by its equivalent circuit. The circuit then becomes as shown in Fig. 1.13. Note that input voltage is applied across the ac resistance of the emitter circuit i.e., (r’e + RE). Assuming the emitter diode to be ideal,

Output voltage, Vout = ie RE

Input voltage, Vin = ie (r’e + RE)

Voltage gain of emitter follower is

\[ A_v = \frac{V_{out}}{V_{in}} = \frac{i_e R_E}{i_e (r'_e + R_E)} = \frac{R_E}{r'_e + R_E} \]

or

\[ A_v = \frac{R_E}{r'_e + R_E} \]
In most practical applications, $R_E \gg r'e$ so that $A_v = 1$.

In practice, the voltage gain of an emitter follower is between 0.8 and 0.999.

### 1.12 Input Impedance of Emitter Follower

Fig. 1.14 (i) shows the circuit of a loaded emitter follower. The a.c. equivalent circuit with T model is shown in Fig. 1.14 (ii).

As for CE amplifier, the input impedance of emitter follower is the combined effect of biasing resistors ($R_1$ and $R_2$) and the input impedance of transistor base [$Z_{in\ (base)}$]. Since these resistances are in parallel to the ac signal, the input impedance $Z_{in}$ of the emitter follower is given by:

\[
Z_m = R_1 \parallel R_2 \parallel Z_{m\ (base)}
\]

where

\[
Z_{in\ (base)} = \beta (r'e + R'_E)
\]

Now

\[
r'e = \frac{25 \text{ mV}}{I_E}
\]

and

\[
R'_E = R_E \parallel R_L
\]
Figure 1.14 (ii)

1.13 Output Impedance of Emitter Follower

The output impedance of a circuit is the impedance that the circuit offers to the load. When load is connected to the circuit, the output impedance acts as the source impedance for the load. Fig.1.15 shows the circuit of emitter follower. Here $R_s$ is the output resistance of amplifier voltage source. It can be proved that the output impedance $Z_{out}$ of the emitter follower is given by:

$$Z_{out} = R_E \parallel \left( r'_e + \frac{R'_m}{\beta} \right)$$

In practical circuits, the value of $R_E$ is large enough to be ignored. For this reason, the output impedance of emitter follower is approximately given by:

$$Z_{out} = r'_e + \frac{R'_m}{\beta} + V_{CC}$$

Figure 1.15
1.14 Applications of Emitter Follower

The emitter follower has the following principal applications:

(i) To provide current amplification with no voltage gain.

(ii) Impedance matching.

(i) Current amplification without voltage gain. We know that an emitter follower is a current amplifier that has no voltage gain ($A_v = 1$). There are many instances (especially in digital electronics) where an increase in current is required but no increase in voltage is needed. In such a situation, an emitter follower can be used. For example, consider the two stage amplifier circuit as shown in Fig. 1.16. Suppose this 2 stage amplifier has the desired voltage gain but current gain of this multistage amplifier is insufficient. In that case, we can use an emitter follower to increase the current gain without increasing the voltage gain.

![Figure 1.16](image)

(ii) Impedance matching. We know that an emitter follower has high input impedance and low output impedance. This makes the emitter follower an ideal circuit for impedance matching. Fig. 1.17 shows the impedance matching by an emitter follower. Here the output impedance of the source is 120 kΩ while that of load is 20 Ω. The emitter follower has an input impedance of 120 kΩ and output impedance of 22 Ω. It is connected between high-impedance source and low impedance load. The net result of this arrangement is that maximum power is transferred from the original source to the original load. When an emitter follower is used for this purpose, it is called a buffer amplifier.

![Figure 1.17](image)

It may be noted that the job of impedance matching can also be accomplished by a transformer. However, emitter follower is preferred for this purpose. It is because emitter follower is not only more convenient than a transformer but it also has much better frequency response i.e., it works well over a large frequency range.
1.15 Nyquist Criterion

Criterion Of Nyquist:

- The $\alpha$ is a function of frequency. Points in the complex plane are obtained for the values of $\alpha$ corresponding to all values of ‘f’ from $-\infty$ to $\infty$. The locus of all these points forms a closed curve.
- The criterion of Nyquist is that amplifier is unstable if this curve encloses the point $(-1+j0)$, and the amplifier is stable if the curve does not enclose this point.

![Nyquist Plot](image)

**Figure 1.18 Nyquist Plot**

The amplifier is unstable if this curve encloses the point $-1+j0$ and the amplifier is stable if the curve does not enclose this point.
UNIT II

OSCILLATORS

2.1 Introduction about Oscillators

An oscillator is a circuit that produces a repetitive signal from a dc voltage. The feedback type oscillator which rely on a positive feedback of the output to maintain the oscillations. The relaxation oscillator makes use of an RC timing circuit to generate a non-sinusoidal signal such as square wave.

The requirements for oscillation are described by the Baukhausen criterion:

- The magnitude of the loop gain $A\beta$ must be 1
- The phase shift of the loop gain $A \beta$ must be $0^\circ$ or $360^\circ$ or integer multiple of $2\pi$

Amplitude stabilization:

- In both the oscillators above, the loop gain is set by component values
- In practice the gain of the active components is very variable
- If the gain of the circuit is too high it will saturate
- If the gain of the circuit is too low the oscillation will die

Real circuits need some means of stabilizing the magnitude of the oscillation to cope with variability in the gain of the circuit

Barkhausan criterion

The conditions for oscillator to produce oscillation are given by Barkhauusen criterion. They are:

- The total phase shift produced by the circuit should be $360^\circ$ or $0^\circ$
- The Magnitude of loop gain must be greater than or equal to 1 (ie)$|A\beta| \geq 1$

In practice loop gain is kept slightly greater than unity to ensure that oscillator work even if there is a slight change in the circuit parameters
2.2 Mechanism of start of oscillation

The starting voltage is provided by noise, which is produced due to random motion of electrons in resistors used in the circuit. The noise voltage contains almost all the sinusoidal frequencies. This low amplitude noise voltage gets amplified and appears at the output terminals. The amplified noise drives the feedback network which is the phase shift network. Because of this the feedback voltage is maximum at a particular frequency, which in turn represents the frequency of oscillation.

**LC Oscillator:**

Oscillators are used in many electronic circuits and systems providing the central “clock” signal that controls the sequential operation of the entire system. Oscillators convert a DC input (the supply voltage) into an AC output (the waveform), which can have a wide range of different wave shapes and frequencies that can be either complicated in nature or simple sine waves depending upon the application.

Oscillators are also used in many pieces of test equipment producing either sinusoidal sine wave, square, sawtooth or triangular shaped waveforms or just a train of pulse of a variable or constant width. LC Oscillators are commonly used in radio-frequency circuits because of their good phase noise characteristics and their ease of implementation.

An Oscillator is basically an Amplifier with “Positive Feedback”, or regenerative feedback (in-phase) and one of the many problems in electronic circuit design is stooping amplifiers from oscillating while trying to get oscillators to oscillate. Oscillators work because they overcome the losses of their feedback resonator circuit either in the form of a capacitor or both in the same circuit by applying DC energy at the required frequency into this resonator circuit.

In other words, an oscillator is a an amplifier which uses positive feedback that generates an output frequency without the use of an input signal.

It is self sustaining. Then an oscillator has a small signal feedback amplifier with an open-loop gain equal too or slightly greater than one for oscillations to start but to continue oscillations the average loop gain must return to unity. In addition to these reactive components, an amplifying device such as an Operational Amplifier or Bipolar Transistors required. Unlike an amplifier there is no external AC input required to cause the Oscillator to work as the DC supply energy is converted by the oscillator into AC energy at the required frequency.

2.3 Basic Oscillator Feedback Circuit

![Basic Oscillator Feedback Circuit Diagram]

Where: $\beta$ is a feedback fraction.
2.3.1 Without Feedback

\[ A_{\text{v}} = \frac{V_{\text{out}}}{V_{\text{in}}} \quad \text{A = open loop voltage gain} \]
\[ A_{\text{v}} \times V_{\text{in}} = V_{\text{out}} \]

2.3.2 With Feedback

\[ A_{\text{v}}(V_{\text{in}} - \beta V_{\text{out}}) = V_{\text{out}} \quad \beta \text{ is the feedback fraction} \]
\[ A_{\text{v}} \times V_{\text{in}} - A_{\text{v}} \beta V_{\text{out}} = V_{\text{out}} \quad A\beta \text{ – the loop gain} \]
\[ A_{\text{v}} \times V_{\text{in}} - V_{\text{out}}(1 + A\beta) \]
\[ G_{\text{v}} = \frac{A}{1 + A\beta} \quad \text{G}_v \text{ = the closed loop gain} \]

Oscillators are circuits that generate a continuous voltage output waveform at a required frequency with the values of the inductors, capacitors or resistors forming a frequency selective LC resonant tank circuit and feedback network. This feedback network is an attenuation network which has a gain of less than one (\( \beta < 1 \)) and starts oscillations when \( A\beta > 1 \) which returns to unity (\( A\beta = 1 \)) once oscillations commence. The LC oscillators frequency is controlled using a tuned or resonant inductive/capacitive (LC) circuit with the resulting output frequency being known as the Oscillation Frequency.

By making the oscillators feedback a reactive network the phase angle of the feedback will vary as a function of frequency and this is called Phase-shift.

There are basically types of Oscillators:

1. Sinusoidal Oscillators - these are known as Harmonic Oscillators and are generally a :LC Tuned-feedback” or “RC tuned-feedback” type Oscillator that generates a purely sinusoidal waveform which is of constant amplitude and frequency.

2. Non-Sinusoidal Oscillators – these are known as Relaxation Oscillators and generate complex non-sinusoidal waveforms that changes very quickly from one condition of stability to another such as “Square-wave”, “Triangular-wave” or “Sawtoothed-wave” type waveforms.

2.3.3 Resonance

When a constant voltage but of varying frequency is applied to a circuit consisting of an inductor, capacitor and resistor the reactance of both the Capacitor/Resistor and Inductor/Resistor circuits is to change both the amplitude and the phase of the output signal due to the reactance of the components used.

At high frequencies the reactance of a capacitor is very low acting as a short circuit while the reactance of the inductor is high acting as an open circuit. At low frequencies the reverse is true, the reactance of the capacitor acts as an open circuit and the reactance of the inductor acts as a short circuit.

Between these two extremes the combination of the inductor and capacitor produces a “Tuned” or “Resonant” circuit that has a Resonant Frequency, (fr) in which the capacitive and inductive reactance’s are equal and cancel out each other, leaving only the resistance of the circuit to oppose the flow of current. This means that there is no phase shift as the current is in phase with the voltage. Consider the circuit below.
2.4 Basic LC Oscillator Tank Circuit

The circuit consists of an inductive coil, L and a capacitor, C. The capacitor stores energy in the form of an electrostatic field and which produces a potential (static voltage) across its plates, while the inductive coil stores its energy in the form of an electromagnetic field.

The capacitor is charged up to the DC supply voltage, V by putting the switch in position A. When the capacitor is fully charged the switch changes to position B. The charged capacitor is now connected in parallel across the inductive coil so the capacitor begins to discharge itself through the coil.

The voltage across C starts falling as the current through the coil begins to rise. This rising current sets up an electromagnetic field around the coil which resists this flow of current. When the capacitor, C is completely discharged the energy that was originally stored in the capacitor, C as an electrostatic filed is now stored in the inductive coil, L as an electromagnetic field around the coils windings.

As there is now no external voltage in the circuit to maintain the current within the coil, it starts to fall as the electromagnetic field begins to collapse. A back emf is induced in the coil (e= -Ldi/dt) keeping the current flowing in the original direction. This current now charges up the capacitor, C with the opposite polarity to its original charge.

C continues to charge up until the current reduces to zero and the electromagnetic field of the coil has collapsed completely. The energy originally introduced into the circuit through the switch, has been returned to the capacitor which again has an electrostatic voltage potential across it, although it is now of the opposite polarity. The capacitor now starts to discharge again back through the coil and the whole process os repeated. The polarity of the voltage changes as the energy is passed back and forth between the capacitor and inductor producing an AC type sinusoidal voltage and current waveform.

This then forms the basis of an LC oscillators tank circuit and theoretically this cycling back and forth will continue indefinitely. However, every time energy is transferred from C to L or from L to C losses occur which decay the oscillations.

This oscillatory action of passing energy back and forth between the capacitor, C to the inductor, L would continue indefinitely if it was not for energy losses within the circuit. Electrical energy is lost in the DC or real resistance of the inductors coil, in the dielectric of the capacitor, and in radiation from the circuit so the oscillation steadily decreases until they die away completely and the process stops.

Then in a practical LC circuit the amplitude of the oscillatory voltage decreases at each half cycle of oscillation and will eventually die away to zero. The oscillations are then said to be "damped" with the amount of damping being determined by the quality or Q-factor of the circuit.
2.41 Damped Oscillations

The frequency of the oscillatory voltage depends upon the value of the inductance and capacitance in the LC tank circuit. We now know that for resonance to occur in the tank circuit, there must be a frequency point were the value of $X_C$, the capacitive reactance is the same as the value of $X_L$, the inductive reactance ($X_L = X_C$) and which will therefore cancel out each other out leaving only the DC resistance in the circuit to oppose the flow of current.

If we now place the curve for inductive reactance on top of the curve for capacitive reactance so that both curves are on the same axes, the point of intersection will give us the resonance frequency point, ($f_r$ or $\omega$) as shown below.

2.4.2 Resonance Frequency

where: $f_r$ is in Hertz, L is in Henries and C is in Farads.

Then the frequency at which this will happen is given as:
\[ X_L = 2\pi f L \quad \text{and} \quad X_C = \frac{1}{2\pi f C} \]

at resonance: \[ X_L = X_C \]

\[ \therefore \quad 2\pi f L = \frac{1}{2\pi f C} \]

\[ 2\pi f^2 L = \frac{1}{2\pi C} \]

\[ \therefore \quad f^2 = \frac{1}{(2\pi)^2 LC} \]

\[ f = \frac{1}{\sqrt{(2\pi)^2 LC}} \]

Then by simplifying the above equation we get the final equation for Resonant Frequency, \( f_r \) in a tuned LC circuit as:

**2.4.3 Resonant Frequency of a LC Oscillator**

\[ f_r = \frac{1}{2\pi \sqrt{LC}} \]

Where:

- L is the Inductance in Henries
- C is the Capacitance in Farads
- \( f_r \) is the Output Frequency in Hertz

This equation shows that if either L or C are decreased, the frequency increases. This output frequency is commonly given the abbreviation of \( f_r \) to identify it as the "resonant frequency". To keep the oscillations going in an LC tank circuit, we have to replace all the energy lost in each oscillation and also maintain the amplitude of these oscillations at a constant level.

The amount of energy replaced must therefore be equal to the energy lost during each cycle. If the energy replaced is too large the amplitude would increase until clipping of the supply rails occurs. Alternatively, if the amount of energy replaced is too small the amplitude would eventually decrease to zero over time and the oscillations would stop.

The simplest way of replacing this lost energy is to take part of the output from the LC tank circuit, amplify it and then feed it back into the LC circuit again. This process can be achieved using a voltage amplifier using an op-amp, FET or bipolar transistor as its active device.

However, if the loop gain of the feedback amplifier is too small, the desired oscillation decays to zero and if it is too large, the waveform becomes distorted. To produce a constant oscillation, the level of the energy fed back to the LC network must be accurately controlled.

Then there must be some form of automatic amplitude or gain control when the amplitude tries to vary from a reference voltage either up or down. To maintain a stable oscillation the overall gain of the circuit must be equal to one or unity. Any less and the oscillations will not start or die away to zero.
any more the oscillations will occur but the amplitude will become clipped by the supply rails causing distortion. Consider the circuit below.

2.5 Basic Transistor LC Oscillator Circuit

![Circuit Diagram]

A Bipolar Transistor is used as the LC oscillators amplifier with the tuned LC tank circuit acts as the collector load. Another coil L2 is connected between the base and the emitter of the transistor whose electromagnetic field is "mutually" coupled with that of coil L. Mutual inductance exists between the two circuits.

The changing current flowing in one coil circuit induces, by electromagnetic induction, a potential voltage in the other (transformer effect) so as the oscillations occur in the tuned circuit, electromagnetic energy is transferred from coil L to coil L2 and a voltage of the same frequency as that in the tuned circuit is applied between the base and emitter of the transistor.

In this way the necessary automatic feedback voltage is applied to the amplifying transistor. The amount of feedback can be increased or decreased by altering the coupling between the two coils L and L2. When the circuit is oscillating its impedance is resistive and the collector and base voltages are 180° out of phase. In order to maintain oscillations (called frequency stability) the voltage applied to the tuned circuit must be "in-phase" with the oscillations occurring in the tuned circuit.

Therefore, we must introduce an additional 180° phase shift into the feedback path between the collector and the base. This is achieved by winding the coil of L2 in the correct direction relative to coil L giving us the correct amplitude and phase relationships for the Oscillators circuit or by connecting a phase shift network between the output and input of the amplifier.

The LC Oscillator is therefore a "Sinusoidal Oscillator" or a "Harmonic Oscillator" as it is more commonly called. LC oscillators can generate high frequency sine waves for use in radio frequency (RF) type applications with the transistor amplifier being of a Bipolar Transistor or FET.

Harmonic Oscillators come in many different forms because there are many different ways to construct an LC filter network and amplifier with the most common being the Hartley LC Oscillator, Colpitts LC Oscillator, Armstrong Oscillator and Clapp Oscillator to name a few.

2.6 The Hartley Oscillator

The main disadvantages of the basic LC Oscillator circuit we looked at in the previous tutorial is that they have no means of controlling the amplitude of the oscillations and also, it is difficult to tune the oscillator to the required frequency.
If the cumulative electromagnetic coupling between L1 and L2 is too small there would be insufficient feedback and the oscillations would eventually die away to zero. Likewise if the feedback was too strong the oscillations would continue to increase in amplitude until they were limited by the circuit conditions producing signal distortion. So it becomes very difficult to "tune" the oscillator.

However, it is possible to feed back exactly the right amount of voltage for constant amplitude oscillations. If we feed back more than is necessary the amplitude of the oscillations can be controlled by biasing the amplifier in such a way that if the oscillations increase in amplitude, the bias is increased and the gain of the amplifier is reduced.

If the amplitude of the oscillations decreases the bias decreases and the gain of the amplifier increases, thus increasing the feedback. In this way the amplitude of the oscillations are kept constant using a process known as Automatic Base Bias.

One big advantage of automatic base bias in a voltage controlled oscillator, is that the oscillator can be made more efficient by providing a Class-B bias or even a Class-C bias condition of the transistor. This has the advantage that the collector current only flows during part of the oscillation cycle so the quiescent collector current is very small.

Then this "self-tuning" base oscillator circuit forms one of the most common types of LC parallel resonant feedback oscillator configurations called the Hartley Oscillator circuit.

### 2.6.1 Hartley Oscillator Tuned Circuit

In the Hartley Oscillator the tuned LC circuit is connected between the collector and the base of the transistor amplifier. As far as the oscillatory voltage is concerned, the emitter is connected to a tapping point on the tuned circuit coil.

The feedback of the tuned tank circuit is taken from the centre tap of the inductor coil or even two separate coils in series which are in parallel with a variable capacitor, C as shown.

The Hartley circuit is often referred to as a split-inductance oscillator because coil L is centre-tapped. In effect, inductance L acts like two separate coils in very close proximity with the current flowing through coil section XY induces a signal into coil section YZ below.

An Hartley Oscillator circuit can be made from any configuration that uses either a single tapped coil (similar to an autotransformer) or a pair of series connected coils in parallel with a single capacitor as shown below.
2.6.2 Basic Hartley Oscillator Circuit

![Hartley Oscillator Circuit Diagram]

When the circuit is oscillating, the voltage at point X (collector), relative to point Y (emitter), is $180^\circ$ out-of-phase with the voltage at point Z (base) relative to point Y. At the frequency of oscillation, the impedance of the Collector load is resistive and an increase in Base voltage causes a decrease in the Collector voltage.

Then there is a 180 phase change in the voltage between the Base and Collector and this along with the original 180 phase shift in the feedback loop provides the correct phase relationship of positive feedback for oscillations to be maintained.

The amount of feedback depends upon the position of the "tapping point" of the inductor. If this is moved nearer to the collector the amount of feedback is increased, but the output taken between the Collector and earth is reduced and vice versa.

Resistors, R1 and R2 provide the usual stabilizing DC bias for the transistor in the normal manner while the capacitors act as DC-blocking capacitors.

In this Hartley Oscillator circuit, the DC Collector current flows through part of the coil and for this reason the circuit is said to be "Series-fed" with the frequency of oscillation of the Hartley Oscillator being given as:

$$f = \frac{1}{2\pi \sqrt{L_T C}}$$

where: $L_T = L_1 + L_2 + 2M$

The frequency of oscillations can be adjusted by varying the "tuning" capacitor, C or by varying the position of the iron-dust core inside the coil (inductive tuning) giving an output over a wide range of frequencies making it very easy to tune. Also the Hartley Oscillator produces an output amplitude which is constant over the entire frequency range.

As well as the Series-fed Hartley Oscillator above, it is also possible to connect the tuned tank circuit across the amplifier as a shunt-fed oscillator as shown below.
2.6.3 Shunt-fed Hartley Oscillator Circuit

In the Shunt-fed Hartley Oscillator both the AC and DC components of the Collector current have separate paths around the circuit. Since the DC component is blocked by the capacitor, C2 no DC flows through the inductive coil, L and less power is wasted in the tuned circuit.

The Radio Frequency Coil (RFC), L2 is an RF choke which has a high reactance at the frequency of oscillations so that most of the RF current is applied to the LC tuning tank circuit via capacitor, C2 as the DC component passes through L2 to the power supply. A resistor could be used in place of the RFC coil, L2 but the efficiency would be less.

2.7 Armstrong oscillator

The Armstrong oscillator (also known as Meissner oscillator) is named after the electrical engineer Edwin Armstrong, its inventor. It is sometimes called a tickler oscillator because the feedback needed to produce oscillations is provided using a tickler coil via magnetic coupling between coil L and coil T.

Assuming the coupling is weak, but sufficient to sustain oscillation, the frequency is determined primarily by the tank circuit (L and C in the illustration) and is approximately given by. In a practical circuit, the actual oscillation frequency will be slightly different from the value provided by this formula because of stray capacitance and inductance, internal losses (resistance), and the loading of the tank circuit by the tickler coil.

This circuit is the basis of the regenerative receiver for amplitude modulated radio signals. In that application, an antenna is attached to an additional tickler coil, and the feedback is reduced, for example, by slightly increasing the distance between coils T and L, so the circuit is just short of oscillation.

The result is a narrow-band radio-frequency filter and amplifier. The non-linear characteristic of the transistor or tube provides the demodulated audio signal.

2.8 The Colpitts Oscillator

The Colpitts Oscillator, named after its inventor Edwin Colpitts is another type of LC oscillator design. In many ways, the Colpitts oscillator is the exact opposite of the Hartley Oscillator we looked at in the previous tutorial. Just like the Hartley oscillator, the tuned tank circuit consists of an LC resonance sub-circuit connected between the collector and the base of a single stage transistor amplifier producing a sinusoidal output waveform.
The basic configuration of the Colpitts Oscillator resembles that of the Hartley Oscillator but the difference this time is that the centre tapping of the tank sub-circuit is now made at the junction of a "capacitive voltage divider" network instead of a tapped autotransformer type inductor as in the Hartley oscillator.

![Colpitts Oscillator Coils](image)

### 2.9 Colpitts Oscillator Circuit

The Colpitts oscillator uses a capacitor voltage divider as its feedback source.

The two capacitors, C1 and C2 are placed across a common inductor, L as shown so that C1, C2 and L forms the tuned tank circuit the same as for the Hartley oscillator circuit.

The advantage of this type of tank circuit configuration is that with less self and mutual inductance in the tank circuit, frequency stability is improved along with a more simple design. As with the Hartley oscillator, the Colpitts oscillator uses a single stage bipolar transistor amplifier as the gain element which produces a sinusoidal output. Consider the circuit below.

### 2.9.1 Basic Colpitts Oscillator Circuit
The transistor amplifiers emitter is connected to the junction of capacitors, C1 and C2 which are connected in series and act as a simple voltage divider. When the power supply is firstly applied, capacitors C1 and C2 charge up and then discharge through the coil L. The oscillations across the capacitors are applied to the base-emitter junction and appear in the amplified at the collector output. The amount of feedback depends on the values of C1 and C2 with the smaller the values of C the greater will be the feedback.

The required external phase shift is obtained in a similar manner to that in the Hartley oscillator circuit with the required positive feedback obtained for sustained un-damped oscillations. The amount of feedback is determined by the ratio of C1 and C2 which are generally "ganged" together to provide a constant amount of feedback so as one is adjusted the other automatically follows.

The frequency of oscillations for a Colpitts oscillator is determined by the resonant frequency of the LC tank circuit and is given as:

\[ f_T = \frac{1}{2\pi \sqrt{LC_T}} \]

where \( C_T \) is the capacitance of C1 and C2 connected in series and is given as:

\[ \frac{1}{C_T} = \frac{1}{C_1} + \frac{1}{C_2} \quad \text{or} \quad C_T = \frac{C_1 \times C_2}{C_1 + C_2} \]

The configuration of the transistor amplifier is of a Common Emitter Amplifier with the output signal 180° out of phase with regards to the input signal. The additional 180° phase shift require for oscillation is achieved by the fact that the two capacitors are connected together in series but in parallel with the inductive coil resulting in overall phase shift of the circuit being zero or 360°. Resistors, R1 and R2 provide the usual stabilizing DC bias for the transistor in the normal manner while the capacitor acts as a DC-blocking capacitors. The radio-frequency choke (RFC) is used to provide a high reactance (ideally open circuit) at the frequency of oscillation, \( f_T \) and a low resistance at DC.

2.9.2 Colpitts Oscillator using an Op-amp

As well as using a bipolar junction transistor (BJT) as the amplifiers active stage of the Colpitts oscillator, we can also use either a field effect transistor, (FET) or an operational amplifier, (op-amp). The operation of an Op-amp Colpitts Oscillator is exactly the same as for the transistorised version with the frequency of operation calculated in the same manner. Consider the circuit below.

2.9.3 Colpitts Oscillator Op-amp Circuit
The advantages of the Colpitts Oscillator over the Hartley oscillators are that the Colpitts oscillator produces a more purer sinusoidal waveform due to the low impedance paths of the capacitors at high frequencies. Also due to these capacitive reactance properties the Colpitts oscillator can operate at very high frequencies into the microwave region.

2.10 RC Phase-Shift Oscillator

In a RC Oscillator the input is shifted $180^\circ$ through the amplifier stage and $180^\circ$ again through a second inverting stage giving us "$180^\circ + 180^\circ = 360^\circ$" of phase shift which is the same as $0^\circ$ thereby giving us the required positive feedback. In other words, the phase shift of the feedback loop should be "$0^\circ$".

In a Resistance-Capacitance Oscillator or simply an RC Oscillator, we make use of the fact that a phase shift occurs between the input to a RC network and the output from the same network by using RC elements in the feedback branch, for example.

**RC Phase-Shift Network**

![RC Phase-Shift Network Diagram]

The circuit on the left shows a single resistor-capacitor network and whose output voltage "leads" the input voltage by some angle less than $90^\circ$. An ideal RC circuit would produce a phase shift of exactly $90^\circ$. The amount of actual phase shift in the circuit depends upon the values of the resistor and the capacitor, and the chosen frequency of oscillations with the phase angle ($\phi$) being given as:

$$\phi = \tan^{-1}\frac{X_C}{R}$$

**RC Oscillator Circuit**

![RC Oscillator Circuit Diagram]
The RC Oscillator which is also called a Phase Shift Oscillator, produces a sine wave output signal using regenerative feedback from the resistor-capacitor combination. This regenerative feedback from the RC network is due to the ability of the capacitor to store an electric charge, (similar to the LC tank circuit).

This resistor-capacitor feedback network can be connected as shown above to produce a leading phase shift (phase advance network) or interchanged to produce a lagging phase shift (phase retard network) the outcome is still the same as the sine wave oscillations only occur at the frequency at which the overall phase-shift is $360^\circ$. By varying one or more of the resistors or capacitors in the phase-shift network, the frequency can be varied and generally this is done using a 3-ganged variable capacitor.

If all the resistors, R and the capacitors, C in the phase shift network are equal in value, then the frequency of oscillations produced by the RC oscillator is given as:

$$f = \frac{1}{2\pi CR\sqrt{6}}$$

### 2.10.1 Op-amp RC Oscillator Circuit

![Op-amp RC Oscillator Circuit](image)

As the feedback is connected to the non-inverting input, the operational amplifier is therefore connected in its "inverting amplifier" configuration which produces the required $180^\circ$ phase shift while the RC network produces the other $180^\circ$ phase shift at the required frequency ($180^\circ + 180^\circ$).

Although it is possible to cascade together only two RC stages to provide the required $180^\circ$ of phase shift ($90^\circ + 90^\circ$), the stability of the oscillator at low frequencies is poor.

One of the most important features of an RC Oscillator is its frequency stability which is its ability too provide a constant frequency output under varying load conditions. By cascading three or even four RC stages together ($4 \times 45^\circ$), the stability of the oscillator can be greatly improved.

RC Oscillators with four stages are generally used because commonly available operational amplifiers come in quad IC packages so designing a 4-stage oscillator with $45^\circ$ of phase shift relative to each other is relatively easy.
2.11 WIEN BRIDGE OSCILLATOR

One of the simplest sine wave oscillators which uses a RC network in place of the conventional LC tuned tank circuit to produce a sinusoidal output waveform, is the Wien Bridge Oscillator.

The Wien Bridge Oscillator is so called because the circuit is based on a frequency-selective form of the Whetstone bridge circuit. The Wien Bridge oscillator is a two-stage RC coupled amplifier circuit that has good stability at its resonant frequency, low distortion and is very easy to tune making it a popular circuit as an audio frequency oscillator

Wien Bridge Oscillator

![Wien Bridge Oscillator Circuit Diagram]

The output of the operational amplifier is fed back to both the inputs of the amplifier. One part of the feedback signal is connected to the inverting input terminal (negative feedback) via the resistor divider network of R1 and R2 which allows the amplifiers voltage gain to be adjusted within narrow limits.

The other part is fed back to the non-inverting input terminal (positive feedback) via the RC Wien Bridge network. The RC network is connected in the positive feedback path of the amplifier and has zero phase shift at just one frequency. Then at the selected resonant frequency, \( f_r \) the voltages applied to the inverting and non-inverting inputs will be equal and "in-phase" so the positive feedback will cancel out the negative feedback signal causing the circuit to oscillate.

Also the voltage gain of the amplifier circuit MUST be equal to three "Gain =3" for oscillations to start. This value is set by the feedback resistor network, R1 and R2 for an inverting amplifier and is given as the ratio \(-R1/R2\).

Also, due to the open-loop gain limitations of operational amplifiers, frequencies above 1MHz are unachievable without the use of special high frequency op-amps. Then for oscillations to occur in a Wien Bridge Oscillator circuit the following conditions must apply.

1. With no input signal the Wien Bridge Oscillator produces output oscillations.
2. The Wien Bridge Oscillator can produce a large range of frequencies.
3. The Voltage gain of the amplifier must be at least 3.
4. The network can be used with a Non-inverting amplifier.
5. The input resistance of the amplifier must be high compared to R so that the RC network is not overloaded and alter the required conditions.
6. The output resistance of the amplifier must be low so that the effect of external loading is minimised.

7. Some method of stabilizing the amplitude of the oscillations must be provided because if the voltage gain of the amplifier is too small the desired oscillation will decay and stop and if it is too large the output amplitude rises to the value of the supply rails, which saturates the op-amp and causes the output waveform to become distorted.

8. With amplitude stabilisation in the form of feedback diodes, oscillations from the oscillator can go on indefinitely.

2.12 Quartz Crystal Oscillators

One of the most important features of any oscillator is its frequency stability, or in other words its ability to provide a constant frequency output under varying load conditions. Some of the factors that affect the frequency stability of an oscillator include: temperature, variations in the load and changes in the DC power supply.

Frequency stability of the output signal can be improved by the proper selection of the components used for the resonant feedback circuit including the amplifier but there is a limit to the stability that can be obtained from normal LC and RC tank circuits.

To obtain a very high level of oscillator stability a Quartz Crystal is generally used as the frequency determining device to produce another types of oscillator circuit known generally as a Quartz Crystal Oscillator, (XO).

![Crystal Oscillator](image)

When a voltage source is applied to a small thin piece of quartz crystal, it begins to change shape producing a characteristic known as the Piezo-electric effect.

This piezo-electric effect is the property of a crystal by which an electrical charge produces a mechanical force by changing the shape of the crystal and vice versa, a mechanical force applied to the crystal produces an electrical charge.

Then, piezo-electric devices can be classed as Transducers as they convert energy of one kind into energy of another (electrical to mechanical or mechanical to electrical).

This piezo-electric effect produces mechanical vibrations or oscillations which are used to replace the LC tank circuit in the previous oscillators.

There are many different types of crystal substances which can be used as oscillators with the most important of these for electronic circuits being the quartz minerals because of their greater mechanical strength.
The quartz crystal used in a Quartz Crystal Oscillator is a very small, thin piece or wafer of cut quartz with the two parallel surfaces metallised to make the required electrical connections. The physical size and thickness of a piece of quartz crystal is tightly controlled since it affects the final frequency of oscillations and is called the crystals "characteristic frequency". Then once cut and shaped, the crystal can not be used at any other frequency. In other words, its size and shape determines its frequency.

The crystals characteristic or resonant frequency is inversely proportional to its physical thickness between the two metallised surfaces. A mechanically vibrating crystal can be represented by an equivalent electrical circuit consisting of low resistance, large inductance and small capacitance as shown below.

**Quartz Crystal**

![Quartz Crystal Equivalent Circuit](image)

The equivalent circuit for the quartz crystal shows an RLC series circuit, which represents the mechanical vibrations of the crystal, in parallel with a capacitance, Cp which represents the electrical connections to the crystal. Quartz crystal oscillators operate at "parallel resonance", and the equivalent impedance of the crystal has a series resonance where Cs resonates with inductance, L and a parallel resonance where L resonates with the series combination of Cs and Cp as shown.

**Crystal Reactance**

The slope of the reactance against frequency above, shows that the series reactance at frequency fs is inversely proportional to Cs because below fs and above fp the crystal appears capacitive, i.e. dX/df, where X is the reactance.
The slope of the reactance against frequency above, shows that the series reactance at frequency $f_s$ is inversely proportional to $C$ because below $f_s$ and above $f_p$ the crystal appears capacitive, i.e. $\frac{dX}{df}$, where $X$ is the reactance. Between frequencies $f_s$ and $f_p$, the crystal appears inductive as the two parallel capacitances cancel out. The point where the reactance values of the capacitances and inductance cancel each other out $X_c = X_L$ is the fundamental frequency of the crystal.

A quartz crystal has a resonant frequency similar to that of a electrically tuned tank circuit but with a much higher Q factor due to its low resistance, with typical frequencies ranging from 4kHz to 10MHz. The cut of the crystal also determines how it will behave as some crystals will vibrate at more than one frequency. Also, if the crystal is not of a parallel or uniform thickness it has two or more resonant frequencies having both a fundamental frequency and harmonics such as second or third harmonics. However, usually the fundamental frequency is more stronger or pronounced than the others and this is the one used. The equivalent circuit above has three reactive components and there are two resonant frequencies, the lowest is a series type frequency and the highest a parallel type resonant frequency.

We have seen in the previous tutorials, that an amplifier circuit will oscillate if it has a loop gain greater or equal to one and the feedback is positive. In a Quartz Crystal Oscillator circuit the oscillator will oscillate at the crystals fundamental parallel resonant frequency as the crystal always wants to oscillate when a voltage source is applied to it.

However, it is also possible to "tune" a crystal oscillator to any even harmonic of the fundamental frequency, (2nd, 4th, 8th etc.) and these are known generally as Harmonic Oscillators while Overtone Oscillators vibrate at odd multiples of the fundamental frequency, 3rd, 5th, 11th etc). Generally, crystal oscillators that operate at overtone frequencies do so using their series resonant frequency.

**Colpitts Crystal Oscillator:**

The design of a Crystal Oscillator is very similar to the design of the Colpitts Oscillator we looked at in the previous tutorial, except that the LC tank circuit has been replaced by a quartz crystal as shown below.

![Colpitts Crystal Oscillator Diagram]

These types of Crystal Oscillators are designed around the common emitter amplifier stage of a Colpitts Oscillator. The input signal to the base of the transistor is inverted at the transistors output. The output signal at the collector is then taken through a 180° phase shifting network which includes the crystal operating in a series resonant mode. The output is also fed back to the input which is "in-phase"
with the input providing the necessary positive feedback. Resistors, R1 and R2 bias the resistor in a Class A type operation while resistor

Re is chosen so that the loop gain is slightly greater than unity.

Capacitors, C1 and C2 are made as large as possible in order that the frequency of oscillations can approximate to the series resonant mode of the crystal and is not dependant upon the values of these capacitors.

The circuit diagram above of the Colpitts Crystal Oscillator circuit shows that capacitors, C1 and C2 shunt the output of the transistor which reduces the feedback signal.

Therefore, the gain of the transistor limits the maximum values of C1 and C2.

The output amplitude should be kept low in order to avoid excessive power dissipation in the crystal otherwise could destroy itself by excessive vibration.

2.13 Pierce Oscillator

The Pierce oscillator is a crystal oscillator that uses the crystal as part of its feedback path and therefore has no resonant tank circuit. The Pierce Oscillator uses a JFET as its amplifying device as it provides a very high input impedance with the crystal connected between the output Drain terminal and the input Gate terminal as shown below.

Pierce Crystal Oscillator

In this simple circuit, the crystal determines the frequency of oscillations and operates on its series resonant frequency giving a low impedance path between output and input.

There is a 180° phase shift at resonance, making the feedback positive. The amplitude of the output sine wave is limited to the maximum voltage range at the Drain terminal.

Resistor, R1 controls the amount of feedback and crystal drive while the voltage across the radio frequency choke, RFC reverses during each cycle. Most digital clocks, watches and timers use a Pierce Oscillator in some form or other as it can be implemented using the minimum of components.
UNIT III

TUNED AMPLIFIERS

3.1 Introduction to tuned circuits

When a radio or television set is turned on, many events take place within the "receiver" before we hear the sound or see the picture being sent by the transmitting station. Many different signals reach the antenna of a radio receiver at the same time. To select a station, the listener adjusts the tuning dial on the radio receiver until the desired station is heard. Within the radio or TV receiver, the actual "selecting" of the desired signal and the rejecting of the unwanted signals are accomplished by means of a tuned circuit.

A tuned circuit consists of a coil and a capacitor connected in series or parallel. Whenever the characteristics of inductance and capacitance are found in a tuned circuit, the phenomenon as RESONANCE takes place.

3.2 Resonance circuits

The frequency applied to an LCR circuit causes XL and XC to be equal, and the circuit is RESONANT. If XL and XC are equal ONLY at one frequency (the resonant frequency). This fact is the principle that enables tuned circuits in the radio receiver to select one particular frequency and reject all others.

This is the reason why so much emphasis is placed on XL and XC. Figure 1-1 shows that a basic tuned circuit consists of a coil and a capacitor, connected either in series, view (A), or in parallel, view (B). The resistance (R) in the circuit is usually limited to the inherent resistance of the components (particularly the resistance of the coil).

Tuned amplifier

- Communication circuit widely uses tuned amplifier and they are used in MW & SW radio frequency 550 KHz – 16 MHz, 54 – 88 MHz, FM 88 – 108 MHz, cell phones 470 - 990 MHz
- Band width is 3 dB frequency interval of pass band and –30 dB frequency interval
- Tune amplifiers are also classified as A, B, C similar to power amplifiers based on conduction angle of devices.
Series resonant circuit

Series resonant features minimum impedance (RS) at resonant.

✓ \( f_r = \frac{1}{2} \sqrt{\frac{1}{LC}} \); \( q = \frac{L}{Rs} \) at resonance \( L=\frac{1}{c} \), \( BW=f_r/Q \)

✓ It behaves as purely resistance at resonance, capacitive below and inductive above resonance

Parallel resonant circuit

✓ Parallel resonance features maximum impedance at resonance = \( \frac{L}{RsC} \)

✓ At resonance \( Fr=\frac{1}{2} \sqrt{\frac{1}{(LC-Rs^2/L^2)}} \); if \( Rs=0 \), \( fr=\frac{1}{2} \sqrt{LC} \)

✓ At resonance it exhibits pure resistance and below \( fr \) parallel circuit exhibits inductive and above capacitive impedance

3.3 Need for tuned circuits:

To understand tuned circuits, we first have to understand the phenomenon of self-induction. And to understand this, we need to know about induction. The first discovery about the interaction between electric current and magnetism was the realization that an electric current created a magnetic field around the conductor. It was then discovered that this effect could be enhanced greatly by winding the conductor into a coil. The effect proved to be two-way: If a conductor, maybe in the form of a coil was placed in a changing magnetic field, a current could be made to flow in it; this is called induction.

So imagine a coil, and imagine that we apply a voltage to it. As current starts to flow, a magnetic field is created. But this means that our coil is in a changing magnetic field, and this induces a current in the coil. The induced current runs contrary to the applied current, effectively diminishing it. We have discovered self-induction. What happens is that the self-induction delays the build-up of current in the coil, but eventually the current will reach its maximum and stabilize at a value only determined by the ohmic resistance in the coil and the voltage applied. We now have a steady current and a steady magnetic field. During the buildup of the field, energy was supplied to the coil, where did that energy go? It went into the magnetic field, and as long as the magnetic field exists, it will be stored there.

Now imagine that we remove the current source. Without a steady current to uphold it, the magnetic field starts to disappear, but this means our coil is again in a variable field which induces a current into it. This time the current is in the direction of the applied current, delaying the decay of the current and the magnetic field till the stored energy is spent. This can give a funny effect: Since the coil must get rid of the stored energy, the voltage over it rises indefinitely until a current can run somewhere! This means you can get a surprising amount of sparks and arching when coils are involved. If the coil is large enough, you can actually get an electric shock from a low-voltage source like an ohmmeter.

3.4 Applications of tuned amplifier

A tuned amplifier is a type of electronic device designed to amplify specific ranges of electrical signals while ignoring or blocking others. It finds common use in devices that work with radio frequency signals such as radios, televisions, and other types of communication equipment; however, it also can be useful in many other applications. Tuned amplifiers can be found in aircraft autopilot systems, audio systems, scientific instruments, spacecraft, or anywhere else there is a need to select and amplify specific electronic signals while ignoring others.

The most common tuned amplifiers an average person interacts with can be found in home or portable entertainment equipment, such as FM stereo receivers. An FM radio has a tuned amplifier that
allows listening to only one radio station at a time. When the knob is turned to change the station, it adjusts a variable capacitor, inductor, or similar device inside the radio, which alters the inductive load of the tuned amplifier circuit. This retunes the amplifier to allow a different specific radio frequency to be amplified so a different radio station can be heard.

3.5 CLASSIFICATION:

1. Single tuned amplifier
2. Double tuned amplifier
3. Stagger tuned amplifier

3.5.1 Single tuned amplifier

Single Tuned Amplifiers consist of only one Tank Circuit and the amplifying frequency range is determined by it. By giving signal to its input terminal of various Frequency Ranges. The Tank Circuit on its collector delivers High Impedance on resonant Frequency. Thus the amplified signal is Completely Available on the output Terminal. And for input signals other than Resonant Frequency, the tank circuit provides lower impedance, hence most of the signals get attenuated at collector Terminal.
R_i - input resistance of the next stage
R_o - output resistance of the generator g_m V_{b'e}
C_c & C_E are negligible small

The equivalent circuit is simplified by

\[ R_s \]
\[ V_s \]
\[ V_i \]
\[ r_{b'e} \]
\[ C_i \]
\[ V_{b'e} \]
\[ g_m V_{b'e} \]
\[ C_{eq} \]
\[ R_0 = h_{oe} \]
\[ R_p \]
\[ V_c \]
\[ R_i \]

Simplified equivalent circuit

\[ C_i = C_{b'e} + C_{p'c} (1 - A) \]
\[ C_{eq} = C_{b'c} \left( \frac{A - 1}{A} \right) + C \]

Where,

A - Voltage gain of the amplifier
C - Tuned circuit capacitance

\[ g_{ce} = \frac{1}{r_{ce}} = h_{oe} - g_m h_{re} \approx h_{oe} = \frac{1}{R_o} \]

3.5.2 Double tuned amplifier

An amplifier that uses a pair of mutually inductively coupled coils where both primary and secondary are tuned, such a circuit is known as “double tuned amplifier”. Its response will provide substantial rejection of frequencies near the pass band as well as relative flat pass band response. The disadvantage of POTENTIAL INSTABILITY in single tuned amplifiers can be overcome in Double tuned amplifiers.

A double tuned amplifier consists of inductively coupled two tuned circuits. One L1, C1 and the other L2, C2 in the Collector terminals. A change in the coupling of the two tuned circuits results in change in the shape of the Frequency response curve.
By proper adjustment of the coupling between the two coils of the two tuned circuits, the required results (High selectivity, high Voltage gain and required bandwidth) may be obtained.

Operation:

The high Frequency signal to be amplified is applied to the input terminal of the amplifier. The resonant Frequency of TUNED CIRCUIT connected in the Collector circuit is made equal to signal Frequency by varying the value of C1. Now the tuned circuit L1, C1 offers very high Impedance to input signal Frequency and therefore, large output is developed across it. The output from the tuned circuit L1, C1 is transferred to the second tuned circuit L2, C2 through Mutual Induction. Hence the Frequency response in Double Tuned amplifier depends on the Magnetic Coupling of L1 and L2.

Equivalent circuit of double tuned amplifier:
Two gain peaks in frequencies $f_1$ and $f_2$

$$f_1 = f_r \left(1 - \frac{1}{2Q \sqrt{k^2 Q^2 - 1}}\right)$$

$$f_2 = f_r \left(1 + \frac{1}{2Q \sqrt{k^2 Q^2 - 1}}\right)$$

This condition is known as critical coupling.

For the values of $k < 1/Q$ the peak gain is less than the maximum gain and the coupling is poor. For the values $k > \frac{1}{Q}$ the circuit is overcoupled and the response shows double peak. This double peak is useful when more bandwidth is required.

The gain magnitude at peak is given as,

$$|A_p| = g_m \omega_0 \sqrt{L_1 L_2} \frac{kQ}{2}$$

And gain at the dip at $\delta = 0$ is given as,

$$|A_d| = |A_p| \frac{2kQ}{1 + k^2 Q^2}$$
The ratio of peak and dip gain is denoted as $\gamma$ and it represents the magnitude of the ripple in the gain curve.

$$\gamma = \left| \frac{A_p}{A_d} \right| = \frac{1 + k^2Q^2}{2kQ}$$

Using quadratic simplification and positive sign

$$kQ = \gamma + \sqrt{\gamma^2 - 1}$$

Bandwidth:

$$BW = 2\delta' = \sqrt{2}(f_2 - f_1)$$

At 3dB Bandwidth

$$3\text{ dB BW} = \frac{3.1f_r}{Q}$$

### 3.5.3 Staggered tuned amplifier

Double tuned amplifier gives greater 3 dB bandwidth having steeper sides and flat top. But alignment of double tuned amplifier is difficult.

To overcome this problem two single tuned cascaded amplifiers having certain bandwidth are taken and their resonant frequencies are so adjusted that they are separated by an amount equal to the bandwidth of each stage. Since the resonant frequencies are displaced or staggered, they are known as staggered tuned amplifiers. If it is desired to build a wide band high gain amplifier, one procedure is to use either single tuned or double tuned circuits which have been heavily loaded so as to increase the bandwidth.

The gain per stage is correspondingly reduced, by virtue of the constant gain-bandwidth product. The use of a cascaded chain of stages will provide for the desired gain. Generally, for a specified gain and bandwidth the double tuned cascaded amplifier is preferred, since fewer tubes are often possible, and also since the pass-band characteristics of the double tuned cascaded chain are more favorable, falling more sensitive to variations in tube capacitance and coil inductance than the single tuned circuits.
Stagger Tuned Amplifiers are used to improve the overall frequency response of tuned Amplifiers. Stagger tuned Amplifiers are usually designed so that the overall response exhibits maximal flatness around the centre frequency. It needs a number of tuned circuits operating in union. The overall frequency response of a Stagger tuned amplifier is obtained by adding the individual response together.
Since the resonant Frequencies of different tuned circuits are displaced or staggered, they are referred as STAGGER TUNED AMPLIFIER.

The main advantage of stagger tuned amplifier is increased bandwidth. Its Drawback is Reduced Selectivity and critical tuning of many tank circuits. They are used in RF amplifier stage in Radio Receivers.

Analysis:

Gain of the single tuned amplifier:

\[
\frac{A_v}{A_v \text{ (at resonance)}_1} = \frac{1}{1+j(X+1)}
\]

\[
\frac{A_v}{A_v \text{ (at resonance)}_2} = \frac{1}{1+j(X-1)}
\]

where \(X = 2 \, Q_{\text{eff}} \delta\)

Gain of the cascaded amplifier:

\[
\frac{A_v}{A_v \text{ (at resonance)}_{\text{cascaded}}} = \frac{A_v}{A_v \text{ (at resonance)}_1} \times \frac{A_v}{A_v \text{ (at resonance)}_2}
\]

\[
\frac{A_v}{A_v \text{ (at resonance)}_{\text{cascaded}}} = \frac{1}{\sqrt{4+(2 \, Q_{\text{eff}} \delta)^4}} = \frac{1}{\sqrt{4+16 \, Q_{\text{eff}}^4 \delta^4}}
\]

\[
= \frac{1}{2\sqrt{1+4 \, Q_{\text{eff}}^4 \delta^4}}
\]
UNIT IV
WAVE SHAPING AND MULTIVIBRATOR CIRCUITS

Linear wave shaping: Process by which the shape of a non sinusoidal signal is changed by passing the signal through the network consisting of linear elements Diodes can be used in wave shaping circuits.

- Either limit or clip signal portion --- clipper
- Shift the DC voltage level of the signal --- clamps

Types of non sinusoidal input

- Step
- Pulse
- Square
- Ramp input

4.1 RL circuit

- RL circuit is used for small time constants.
- To get a large time constant the inductance value has to be chosen high
- Higher inductance value are provided by iron core inductors which are bigger in size, heavy and costly.

![RL Circuit Diagram]

4.2 The RC Integrator

The Integrator is basically a low pass filter circuit operating in the time domain that converts a square wave "step" response input signal into a triangular shaped waveform output as the capacitor charges and discharges.

A Triangular waveform consists of alternate but equal, positive and negative ramps. As seen below, if the RC time constant is long compared to the time period of the input waveform the resultant output waveform will be triangular in shape and the higher the input frequency the lower will be the output amplitude compared to that of the input.
This then makes this type of circuit ideal for converting one type of electronic signal to another for use in wave-generating or wave-shaping circuits.

**The Low Pass Filter**

A simple passive Low Pass Filter or LPF, can be easily made by connecting together in series a single Resistor with a single Capacitor as shown below. In this type of filter arrangement the input signal (Vin) is applied to the series combination (both the Resistor and Capacitor together) but the output signal (Vout) is taken across the capacitor only.

This type of filter is known generally as a "first-order filter" or "one-pole filter", why first-order or single-pole, because it has only "one" reactive component in the circuit, the capacitor.

**Low Pass Filter Circuit**

The reactance of a capacitor varies inversely with frequency, while the value of the resistor remains constant as the frequency changes. At low frequencies the capacitive reactance, (Xc) of the capacitor will be very large compared to the resistive value of the resistor, R and as a result the voltage across the capacitor, Vc will also be large while the voltage drop across the resistor, Vr will be much lower. At high frequencies the reverse is true with Vc being small and Vr being large.

**High Pass Filters**

A High Pass Filter or HPF, is the exact opposite to that of the Low Pass filter circuit, as now the two components have been interchanged with the output signal (Vout) being taken from across the resistor as shown.

Where the low pass filter only allowed signals to pass below its cut-off frequency point, fc. The passive high pass filter circuit as its name implies, only passes signals above the selected cut-off point, fc eliminating any low frequency signals from the waveform. Consider the circuit below.
The High Pass Filter Circuit

![High Pass Filter Circuit Diagram](image)

In this circuit arrangement, the reactance of the capacitor is very high at low frequencies so the capacitor acts like an open circuit and blocks any input signals at Vin until the cut-off frequency point (fc) is reached.

Above this cut-off frequency point the reactance of the capacitor has reduced sufficiently as to now act more like a short circuit allowing all of the input signal to pass directly to the output as shown below in the High Pass Frequency Response Curve.

**RC Differentiator**

Up until now the input waveform to the filter has been assumed to be sinusoidal or that of a sine wave consisting of a fundamental signal and some harmonics operating in the frequency domain giving us a frequency domain response for the filter.

However, if we feed the **High Pass Filter** with a **Square Wave** signal operating in the time domain giving an impulse or step response input, the output waveform will consist of short duration pulse or spikes as shown.

![Square Wave Input Signal](image)

Each cycle of the square wave input waveform produces two spikes at the output, one positive and one negative and whose amplitude is equal to that of the input. The rate of decay of the spikes depends upon the time constant, (RC) value of both components, \(t = R \times C\) and the value of the input frequency. The output pulses resemble more and more the shape of the input signal as the frequency increases

**4.3 RL INTEGRATORS:**

The RL circuit may also be used as an integrating circuit. An integrated waveform may be obtained from the series RL circuit by taking the output across the resistor. The characteristics of the inductor are such that at the first instant of time in which voltage is applied, current flow through the inductor is minimum and the voltage developed across it is maximum.
Therefore, the value of the voltage drop across the series resistor at that first instant must be \( V \) volts because there is no current flow through it. As time passes, current begins to flow through the circuit and voltage develops across the resistor. Since the circuit has a long time constant, the voltage across the resistor does NOT respond to the rapid changes in voltage of the input square wave. Therefore, the conditions for integration in an RL circuit are a long time constant with the output taken across the resistor.

There are a variety of diode network called clippers that have the ability to “clip” off a portion of the input signal without distorting the remaining part of the alternating waveform. The half wave rectifier is an example of the simplest form of diode clipper one resistor and diode.

Depending on the orientation of the diode, the positive or negative region of the input signal is “clipped” off. There are two general categories of clippers: series and parallel. The series configuration is defined as one where the diode is in series with the load, while the parallel variety has the diode in a branch parallel to the load.

### 4.4 Multivibrators

#### Introduction

The type of circuit most often used to generate square or rectangular waves is the multivibrator. A multivibrator, is basically two amplifier circuits arranged with regenerative feedback. One of the amplifiers is conducting while the other is cut off. When an input signal to one amplifier is large enough, the transistor can be driven into cutoff, and its collector voltage will be almost \( V_{CC} \). However, when the transistor is driven into saturation, its collector voltage will be about 0 volts.

A circuit that is designed to go quickly from cutoff to saturation will produce a square or rectangular wave at its output. This principle is used in multivibrators. Multivibrators are classified according to the number of steady (stable) states of the circuit. A steady state exists when circuit operation is essentially constant; that is, one transistor remains in conduction and the other remains cut off until an external signal is applied.

The three types of multivibrators:

- **ASTABLE**
- **MONOSTABLE**
- **BISTABLE**.

The astable circuit has no stable state. With no external signal applied, the transistors alternately switch from cutoff to saturation at a frequency determined by the RC time constants of the coupling circuits.

The monostable circuit has one stable state; one transistor conducts while the other is cut off. A signal must be applied to change this condition. After a period of time, determined by the internal RC components, the circuit will return to its original condition where it remains until the next signal arrives.

The bistable multivibrator has two stable states. It remains in one of the stable states until a trigger is applied. It then flips to the other stable condition and remains there until another trigger is applied. The multivibrator then changes back (FLOPS) to its first stable state.

### 4.4.1 Astable Multivibrator

A multivibrator which generates square waves of its own (i.e. without any external trigger pulse) is known as astable multivibrator. It is also called free running multivibrator. It has no stable state but
only two quasi-stables (half-stable) makes oscillating continuously between these states. Thus it is just an oscillator since it requires no external pulse for its operation of course it does require D.C power.

In such circuit neither of the two transistors reaches a stable state. It switches back and forth from one state to the other, remaining in each state for a time determined by circuit constants. In other words, at first one transistor conducts (i.e. ON state) and the other stays in the OFF state for some time. After this period of time, the second transistor is automatically turned ON and the first transistor turned OFF. Thus the multivibrator will generate a square wave of its own. The width of the square wave and it frequency will depend upon the circuit constants.

Here we like to describe.

- Collector - coupled Astable multivibrator
- Emitter - coupled Astable multivibrator

Figure (a) shows the circuit of a collector coupled astable multivibrator using two identical NPN transistors Q₁ and Q₂. It is possible to have \( R_{L1} = R_{L2} = R_L = R_1 = R_2 = R \) and \( C_1 = C_2 = C \). In that case, the circuit is known as symmetrical astable multivibrator. The transistor Q₁ is forward biased by the \( V_{cc} \) supply through resistor \( R_2 \). Similarly the transistor Q₂ is forward biased by the \( V_{cc} \) supply through resistor \( R_1 \). The output of transistor Q₁ is coupled to the input of transistor Q₂ through the capacitor \( C_2 \). Similarly the output of transistor Q₂ is coupled to the input of transistor Q₁ through the capacitor \( C_1 \).

![Figure (a)](image)

It consists of two common emitter amplifying stages. Each stage provides a feedback through a capacitor at the input of the other. Since the amplifying stage introduces a 180° phase shift and another 180° phase shift is introduced by a capacitor, therefore the feedback signal and the circuit works as an oscillator. In other words because of capacitive coupling none of the transistor can remain permanently out-off or saturated, instead of circuit has two quasi-stable states (ON and OFF) and it makes periodic transition between these two states.
The output of an Astable multivibrator is available at the collector terminal of the either transistors as shown in figure (a). However, the two outputs are 180° out of phase with each other. Therefore one of the outputs is said to be the complement of the other.

Let us suppose that

When \( Q_1 \) is ON, \( Q_2 \) is OFF and

When \( Q_2 \) is ON, \( Q_1 \) is OFF.

When the D.C power supply is switched ON by closing \( S \), one of the transistors will start conducting before the other (or slightly faster than the other). It is so because characteristics of no two similar transistors can be exactly alike suppose that \( Q_1 \) starts conducting before \( Q_2 \) does. The feedback system is such that \( Q_1 \) will be very rapidly driven ton saturation and \( Q_2 \) to cut-off. The circuit operation may be explained as follows.

Since \( Q_1 \) is in saturation whole of \( V_{CC} \) drops across \( R_{L1} \). Hence \( V_{C1} = 0 \) and point A is at zero or ground potential. Since \( Q_2 \) is in cut-off i.e. it conducts no current, there is no drop across \( R_{L2} \). Hence point B is at \( V_{CC} \). Since A is at 0V \( C_2 \) starts to charge through \( R_2 \) towards \( V_{CC} \).

When voltage across \( C_2 \) rises sufficiently (i.e. more than 0.7V), it biases \( Q_2 \) in the forward direction so that it starts conducting and is soon driven to saturation.

\( V_{CC} \) decreases and becomes almost zero when \( Q_2 \) gets saturated. The potential of point B decreases from \( V_{CC} \) to almost 0V. This potential decrease (negative swing) is applied to the base of \( Q_1 \) through \( C_1 \). Consequently, \( Q_1 \) is pulled out of saturation and is soon driven to cut-off.

Since, now point B is at 0V, \( C_1 \) starts charging through \( R_1 \) towards the target voltage \( V_{CC} \).

When voltage of \( C_1 \) increases sufficiently, \( Q_1 \) becomes forward-biased and starts conducting. In this way the whole cycle is repeated.

It is observed that the circuit alternates between a state in which \( Q_1 \) is ON and \( Q_2 \) is OFF and the state in which \( Q_1 \) is OFF and \( Q_2 \) is ON. This time in each state depends on RC values. Since each transistor is driven alternately into saturation and cut-off. The voltage waveform at either collector (points A and B in figure (b)) is essentially a square waveform with peak amplitude equal to \( V_{CC} \).

**Calculation of switching times and frequency of oscillations:**

The frequency of oscillations can be calculated by charging and discharging capacitances and its base resistance \( R_B \).

The voltage across the capacitor can be written as

\[
V_a = V_f - (V_f - V_i) e^{-\frac{t}{RC}} = V_s
\]

\( V_i \) = intial voltage = \( V_B = -V_{CC} \) thus the transistors enters from ON to OFF state

\( V_f \) = final voltage = \( V_B = -V_{CC} \) then the resistor enters from OFF to ON state

\( T_1 \) is ON & \( T_2 \) is OFF the above equation can be written as
\[ V_{B1} = V_{CC} \left[ 1 - 2e^{-t/R_{B2}C_2} \right] \]

substitute at \( t=T_1 \), \( V_{B1}=0 \) hence this equation becomes

\[ T_1 = 0.69R_{B2}C_2 \]

The total time period \( T = 0.694(R_{B1}C_1 + R_{B2}C_2) \)

When \( R_{B1} = R_{B2} = R \) & \( C_1 = C_2 = C \)

\[ T = 1.39RC \]

Frequency of free running multivibrator is given by

\[ F = \frac{1}{\text{total time period}(T)} = \frac{1}{1.39RC} = \frac{0.7}{RC} \]

the frequency stability of the circuit is not good as only the function of the product of RC but also depends on load resistances, supply voltages and circuit parameters. In order to stabilize the frequency, synchronizing signals are injected which terminate the unstable periods earlier than would occur naturally.

### 4.4.2 Bistable Multivibrator

The bistable multivibrator has two absolutely stable states. It will remain in whichever state it happens to be until a trigger pulse causes it to switch to the other state. For instance, suppose at any particular instant, transistor \( Q_1 \) is conducting and transistor \( Q_2 \) is at cut-off. If left to itself, the bistable multivibrator will stay in this position for ever. However, if an external pulse is applied to the circuit in such a way that \( Q_1 \) is cut-off and \( Q_2 \) is turned on, the circuit will stay in the new position. Another trigger pulse is then required to switch the circuit back to its original state.

In other words a multivibrator which has both the state stable is called a bistable multivibrator. It is also called flip-flop, trigger circuit or binary. The output pulse is obtained when, and why a driving (triggering) pulse is applied to the input. A full cycle of output is produced for every two triggering pulses of correct polarity and amplitude.
Figure (a) shows the circuit of a bistable multivibrator using two NPN transistors. Here the output of a transistor Q_2 is coupled out of a transistor Q_1 through a resistor R_2. Similarly, the output of a transistor Q_1 is coupled to the base of transistor Q_2 through a resistor R_1. The capacitors C_2 and C_1 are known as speed up capacitors. Their function is to increase the speed of the circuit in making abrupt transition from one stable state to another stable state. The base resistors (R_3 and R_4) of both the transistors are connected to a common source (-V_{BB}). The output of a bistable multivibrator is available at the collector terminal of both the transistor Q_1 and Q. However, the two outputs are the complements of each other.

Let us suppose, if Q_1 is conducting, then the fact that point A is at nearly ON makes the base of Q_2 negative (by the potential divider R_2 - R_4) and holds Q_2 off.

Similarly with Q_2 OFF, the potential divider from V_{CC} to -V_{BB} (R_{L2}, R_1, R_3) is designed to keep base of Q_1 at about 0.7V ensuring that Q_1 conducts. It is seen that Q_1 holds Q_2 OFF and Q_2 hold Q_1 ON. Suppose, now a positive pulse is applied momentarily to R. It will cause Q_2 to conduct. As collector of Q_2 falls to zero, it cuts Q_1 OFF and consequently, the BMV switches over to its other state.

Similarly, a positive trigger pulse applied to S will switch the BMV back to its original state.

Uses:

- In timing circuits as frequency divider
- In counting circuits
- In computer memory circuits

**Bistable Multivibrator Triggering**

To change the stable state of the binary it is necessary to apply an appropriate pulse in the circuit, which will try to bring both the transistors to active region and the resulting regenerative feedback will result on the change of state.

Triggering may be of two following types:

- Asymmetrical triggering
- Symmetrical triggering

(I) Asymmetrical triggering

In asymmetrical triggering, there are two trigger inputs for the transistors Q_1 and Q_2. Each trigger input is derived from a separate triggering source. To induce transition among the stable states, let us say that initially the trigger is applied to the bistable. For the next transition, now the identical trigger must appear at the transistor Q_2. Thus it can be said that the asymmetrical triggering the trigger pulses derived from two separate source and connected to the two transistors Q_1 and Q_2 individually, sequentially change the state of the bistable.

Figure (b) shows the circuit diagram of an asymmetrical triggered bistable multivibrator.
Initially $Q_1$ is OFF and transistor $Q_2$ is ON. The first pulse derived from the trigger source A, applied to the terminal turn it OFF by bringing it from saturation region to active transistor $Q_1$ is ON and transistor $Q_2$ is OFF. Any further pulse next time then the trigger pulse is applied at the terminal B, the change of stable state will result with transistor $Q_2$ On and transistor $Q_1$ OFF.

Asymmetrical triggering finds its application in the generation of a gate waveform, the duration of which is controlled by any two independent events occurring at different time instants. Thus measurement of time interval is facilitated.

(II) symmetrical triggering

There are various symmetrical triggering methods called symmetrical collector triggering, symmetrical base triggering and symmetrical hybrid triggering. Here we would liked to explain only symmetrical base triggering (positive pulse) only as given under symmetrical Base Triggering.
Figure (c) shows the circuit diagram of a binary with symmetrical base triggering applying a positive trigger pulses.

Diodes $D_1$ and $D_2$ are steering diodes. Here the positive pulses, try to turn ON and OFF transistor. Thus when transistor $Q_1$ is OFF and transistor $Q_2$ is ON, the respective base voltages and $V_{B1N, \text{OFF}}$ and $V_{B2N, \text{ON}}$. It will be seen that $V_{B1N, \text{OFF}} > V_{B1N, \text{ON}}$. Thus diode $D_2$ is more reverse-biased compared to diode $D_1$.

When the positive differentiated pulse of amplitude greater than $(V_{B1N, \text{OFF}} + V_{\gamma})$ appears, the diode $D_1$ gets forward biased, and transistor $Q_1$ enters the active region and with subsequent regenerative feedback $Q_1$ gets ON, and transistor $Q_2$ becomes OFF. On the arrival of the next trigger pulse now the diode $D_2$ will be forward biased and ultimately with regenerative feedback it will be in the ON state.

4.5 Clippers

4.5.1 Series clipper

The response of the series configuration to a variety of alternating waveforms is provided although first introduced as a half-wave rectifier (for sinusoidal waveforms); there are no boundaries on the type of signals that can be applied to a clipper. The addition of a dc supply can have a pronounced effect on the output of a clipper. Our initial discussion will be limited to ideal diodes, with the effect of $V_T$ reserved for a concluding example.

Circuit diagram:

Waveform:

Series clipper with dc supply
There is no general procedure for analyzing networks such as the type in Fig but there are a few thoughts to keep in mind as you work toward a solution. Make a mental sketch of the response of the network based on the direction of the diode and the applied voltage levels. For the network, the direction of the diode suggests that the signal must be positive to turn it on. The dc supply further requires that the voltage be greater than V volts to turn the diode on.

The negative region of the input signal is —pressuring the diode into the —off state, supported further by the dc supply. In general, therefore, we can be quite sure that the diode is an open circuit (—off state) for the negative region of the input signal. Determine the applied voltage (transition voltage) that will cause a change in state for the diode: For an input voltage greater than V volts the diode is in the short-circuit state, while for input voltages less than V volts it is in the open-circuit or —off state.

Determining the transition level for the circuit

Be continually aware of the defined terminals and polarity of Vo. When the diode is in the short-circuit state, such as shown in Fig., the output voltage Vo can be determined by applying Kirchhoff’s voltage law in the clockwise direction Vi – V – Vo (CW direction)

It can be helpful to sketch the input signal above the output and determine the output at instantaneous values of the input:
It is then possible that the output voltage can be sketched from the resulting data points of as demonstrated. Keep in mind that at an instantaneous value of \( v_i \) the input can be treated as a dc supply of that value and the corresponding dc value (the instantaneous value) of the output determined. For instance, at \( v_i = V_m \) for the network, the network to be analyzed appears. For \( V_m > V \) the diode is in the short-circuit state and \( V_o = V_m - V \).

Determining Levels Of \( V_o \)

Determining \( V_o \) When \( v_i = V_m \)

At the \( v_i = V_m \) diodes change state; at \( v_i = -V_m \), \( V_o = 0 \); and the complete curve for \( V_o \) can be sketched.

4.6 Clamper

The clamping network is one that will—clamp a signal to a different dc level. The network must have a capacitor, a diode, and a resistive element, but it can also employ an independent dc supply to introduce an additional shift. The magnitude of \( R \) and \( C \) must be chosen such that the time constant \( \tau = RC \) is large enough to ensure that the voltage across the capacitor does not discharge significantly during the interval the diode is non conducting.

Throughout the analysis we will assume that for all practical purposes the capacitor will fully charge or discharge in five time constants. The network of Fig. will clamp the input signal to the zero level (for ideal diodes). The resistor \( R \) can be the load resistor or a parallel combination of the load resistor and a resistor designed to provide the desired level of \( R \).
Clamper

Diode —on and the capacitor charging to V volts.

During the interval $0 \rightarrow T/2$ the network will appear, with the diode in the —on state effectively —shorting out the effect of the resistor $R$. The resulting RC time constant is so small ($R$ determined by the inherent resistance of the network) that the capacitor will charge to $V$ volts very quickly. During this interval the output voltage is directly across the short circuit and $V_o = 0$ V. When the input switches to the $-V$ state, the network will appear With an open circuit equivalent for the diode determined by the applied signal and stored voltage across the capacitor—both —pressuring current through the diode from cathode to anode.

Now that $R$ is back in the network the time constant determined by the RC product is sufficiently large to establish a discharge period much greater than the period $T/2 \rightarrow T$, and it can be assumed on an approximate basis that the capacitor holds onto all its charge and, therefore, voltage (since $V = Q/C$) during this period. Since $vo$ is in parallel with the diode and resistor, it can also be drawn in the alternative position shown in Fig. 2.94. Applying Kirchhoff’s voltage law around the input loop will result in $-V – V – V_o = 0$ and $V_o = 2V$

Determining $V_o$ with the diode —off.
Sketching Vo for the network

The negative sign resulting from the fact that the polarity of 2V is opposite to the polarity defined for Vo. The resulting output waveform appears with the input signal. The output signal is clamped to 0 V for the interval 0 to T/2 but maintains the same total swing (2V) as the input. For a clamping network:

The total swing of the output is equal to the total swing of the input signal.

This fact is an excellent checking tool for the result obtained. In general, the following steps may be helpful when analyzing clamping networks:

1. Start the analysis of clamping systems by considering that part of the input signal that will forward bias the diode. The statement above may require skipping an interval of the input signal (as demonstrated in an example to follow), but the analysis will not be extended by an unnecessary measure of investigation. During the period that the diode is in the —on state, assume that the capacitor will charge up instantaneously to a voltage level determined by the network.

3. Assume that during the period when the diode is in the —off state the capacitor will hold on to its established voltage level.

4. Throughout the analysis maintain a continual awareness of the location and reference polarity for to ensure that the proper levels for are obtained.

5. Keep in mind the general rule that the total swing of the total output must match the swing of the input signal.

4.6.1 Positive Clamper

During the negative half cycle of the input signal, the diode conducts and acts like a short circuit. The output voltage Vo 0 volts. The capacitor is charged to the peak value of input voltage Vm. and it behaves like a battery. During the positive half of the input signal, the diode does not conduct and acts as an open circuit. Hence the output voltage Vo= Vm+ Vm This gives a positively clamped voltage
4.6.2 Negative Clamper

During the positive half cycle the diode conducts and acts like a short circuit. The capacitor charges to peak value of input voltage $V_m$. During this interval the output $V_o$ which is taken across the short circuit will be zero. During the negative half cycle, the diode is open. The output voltage can be found by applying KVL.

$$V_o = -2V_m$$

4.7 Schmitt Trigger

Sometimes an input signal to a digital circuit doesn't directly fit the description of a digital signal. For various reasons it may have slow rise and/or fall times, or may have acquired some noise that could be sensed by further circuitry. It may even be an analog signal whose frequency we want to measure. All of these conditions, and many others, require a specialized circuit that will "clean up" a signal and force it to true digital shape.
The required circuit is called a Schmitt Trigger. It has two possible states just like other multivibrators. However, the trigger for this circuit to change states is the input voltage level, rather than a digital pulse. That is, the output state depends on the input level, and will change only as the input crosses a pre-defined threshold.

Unlike the other multivibrators you have built and demonstrated, the Schmitt Trigger makes its feedback connection through the emitters of the transistors as shown in the schematic diagram to the right. This makes for some useful possibilities, as we will see during our discussion of the operating theory of this circuit.

To understand how this circuit works, assume that the input starts at ground, or 0 volts. Transistor Q1 is necessarily turned off, and has no effect on this circuit. Therefore, RC1, R1, and R2 form a voltage divider across the 5 volt powersupply to set the base voltage of Q2 to a value of $5 \times (R2)/(RC1 + R1 + R2)$. If we assume that the two transistors are essentially identical, then as long as the input voltage remains significantly less than the base voltage of Q2, Q1 will remain off and the circuit operation will not change.

While Q1 is off, Q2 is on. Its emitter and collector current are essentially the same, and are set by the value of RE and the emitter voltage, which will be less than the Q2 base voltage by $V_{BE}$. If Q2 is in saturation under these circumstances, the output voltage will be within a fraction of the threshold voltage set by RC1, R1, and R2. It is important to note that the output voltage of this circuit cannot drop to zero volts, and generally not to a valid logic 0. We can deal with that, but we must recognize this fact.

Now, suppose that the input voltage rises, and continues to rise until it approaches the threshold voltage on Q2's base. At this point, Q1 begins to conduct. Since it now carries some collector current, the current through RC1 increases and the voltage at the collector of Q1 decreases. But this also affects our voltage divider, reducing the base voltage on Q2. But since Q1 is now conducting it carries some of the current flowing through RE, and the voltage across RE doesn't change as rapidly. Therefore, Q2 turns off and the output voltage rises to +5 volts. The circuit has just changed states.

If the input voltage rises further, it will simply keep Q1 turned on and Q2 turned off. However, if the input voltage starts to fall back towards zero, there must clearly be a point at which this circuit will reset itself. The question is, What is the falling threshold voltage? It will be the voltage at which Q1's base becomes more negative than Q2's base, so that Q2 will begin conducting again. However, it isn't the same as the rising threshold voltage, since Q1 is currently affecting the behavior of the voltage divider.

We won't go through all of the derivation here, but when $V_{IN}$ becomes equal to Q2's base voltage, Q2's base voltage will be:

As $V_{IN}$ approaches this value, Q2 begins to conduct, taking emitter current away from Q1. This reduces the current through RC1 which raises Q2's base voltage further, increasing Q2's forward bias and decreasing Q1's forward bias. This in turn will turn off Q1, and the circuit will switch back to its original state.

Three factors must be recognized in the Schmitt Trigger. First, the circuit will change states as $V_{IN}$ approaches $V_{B2}$, not when the two voltages are equal. Therefore $V_{B2}$ is very close to the threshold voltage, but is not precisely equal to it. For example, for the component values shown above, $V_{B2}$ will be 2.54 volts when Q1 is held off, and 2.06 volts as $V_{IN}$ is falling towards this value.
Second, since the common emitter connection is part of the feedback system in this circuit, RE must be large enough to provide the requisite amount of feedback, without becoming so large as to starve the circuit of needed current. If RE is out of range, the circuit will not operate properly, and may not operate as anything more than a high-gain amplifier over a narrow input voltage range, instead of switching states.

The third factor is the fact that the output voltage cannot switch over logic levels, because the transistor emitters are not grounded. If a logic-level output is required, which is usually the case, we can use a circuit such as the one shown here to correct this problem. This circuit is basically two RTL inverters, except that one uses a PNP transistor. This works because when Q2 above is turned off, it will hold a PNP inverter off, but when it is on, its output will turn the PNP transistor on. The NPN transistor here is a second inverter to re-invert the signal and to restore it to active pull-down in common with all of our other logic circuits.

The circuit you will construct for this experiment includes both of the circuits shown here, so that you can monitor the response of the Schmitt trigger with L0.

**Schmitt Waveform Generators**

Simple **Waveform Generators** can be constructed using basic Schmitt trigger action Inverters such as the TTL 74LS14. This method is by far the easiest way to make a basic astable waveform generator. When used to produce clock or timing signals, the astable multivibrator must produce a stable waveform that switches quickly between its "HIGH" and "LOW" states without any distortion or noise, and Schmitt inverters do just that.

We know that the output state of a Schmitt inverter is the opposite or inverse to that of its input state, (NOT Gate principles) and that it can change state at different voltage levels giving it "hysteresis". Schmitt inverters use a Schmitt Trigger action that changes state between an upper and a lower threshold level as the input voltage signal increases and decreases about the input terminal. This upper threshold level "sets" the output and the lower threshold level"resets" the output which equates to a logic "0" and a logic "1" respectively for an inverter. Consider the circuit below.

**TTL Schmitt Waveform Generator**

The circuit consists simply of a TTL 74LS14 Schmitt inverter logic gate with a capacitor, C connected between its input terminal and ground, (0v) with the positive feedback required for the circuit to oscillate is provided by the feedback resistor, R. So how does it work?. Assume that the charge across the capacitors plates is below the Schmitt’s lower threshold level of 0.8 volt (Datasheet value). This therefore makes the input to the inverter at a logic "0" level resulting in a logic "1" output level (inverter principals). One side of the resistor R is now connected to the logic "1" level (+5V) output while the other side of the resistor is connected to the capacitor, C which is at a logic "0" level (0.8v or below).

The capacitor now starts to charge up in a positive direction through the resistor at a rate determined by the RC time constant of the combination. When the charge across the capacitor reaches the 1.6 volt upper threshold level of the Schmitt trigger (Datasheet value) the output from the Schmitt inverter changes rapidly from a logic level "1" to a logic level "0" state and the current flowing through the resistor changes direction.

This change now causes the capacitor that was originally charging up through the resistor, R to begin to discharge itself back through the same resistor until the charge across the capacitors plates reaches the lower threshold level of 0.8 volts and the inverters output switches state again with the cycle repeating itself over and over again as long as the supply voltage is present.
So the capacitor, C is constantly charging and discharging itself during each cycle between the upper and lower threshold levels of the Schmitt inverter producing a logic level "1" or a logic level "0" at the inverter's output. However, the output square wave signal is not symmetrical producing a duty cycle of about 33% or 1/3 as the mark-to-space ratio between "HIGH" and "LOW" is 1:2 respectively due to the input gate characteristics of the TTL inverter.

The value of the feedback resistor, R MUST also be kept low to below 1kΩ for the circuit to oscillate correctly, 220Ω to 470Ω is good, and by varying the value of the capacitor, C to vary the frequency. Also at high frequency levels the output waveform changes shape from a square shaped waveform to a trapezoidal shaped waveform as the input characteristics of the TTL gate are affected by the rapid charging and discharging of the capacitor.

With a resistor value between: 100Ω to 1kΩ, and a capacitor value of between: 1nF to 1000uF. This would give a frequency range of between 1Hz to 1MHz, (high frequencies produce waveform distortion).
UNIT V

BLOCKING OSCILLATORS AND TIMEBASE GENERATORS

5.1 Waveform Generator

Nonsinusoidal oscillators generate complex waveforms such as those just discussed. Because the outputs of these oscillators are generally characterized by a sudden change, or relaxation, these oscillators are often called RELAXATION OSCILLATORS. The pulse repetition rate of these oscillators is usually governed by the charge and discharge timing of a capacitor in series with a resistor.

However, some oscillators contain inductors that along with circuit resistance, affect the output frequency. These RC and LC networks within oscillator circuits are used for frequency determination. Within this category of relaxation oscillators are MULTIVIBRATORS, BLOCKING OSCILLATORS, and SAWTOOTH- and TRAPEZOIDAL-WAVE GENERATORS. Many electronic circuits are not in an "on" condition all of the time. In computers, for example, waveforms must be turned on and off for specific lengths of time.

The time intervals vary from tenths of microseconds to several thousand microseconds. Square and rectangular waveforms are normally used to turn such circuits on and off because the sharp leading and trailing edges make them ideal for timing purposes.

5.2 Time-Base Generators

Radar sets, oscilloscopes, and computer circuits all use sawtooth (voltage or current) waveforms. A sawtooth waveshape must have a linear rise. The sawtooth waveform is often used to produce a uniform, progressive movement of an electron beam across the face of an electrostatic cathode ray tube.

This movement of the electron beam is known as a SWEEP. The voltage which causes this movement is known as SWEEP VOLTAGE and the circuit which produces this voltage is the SWEEP GENERATOR, or TIME-BASE GENERATOR.

Most common types of time-base generators develop the sawtooth waveform by using some type of switching action with either the charge or discharge of an RC or RL circuit.

Sawtooth Wave

A sawtooth wave can be generated by using an RC network. Possibly the simplest sawtooth generator. Assume that at T0, S1 is placed in position P. At the instant the switch closes, the applied voltage (Ea) appears at R. C begins to charge to E through R. If S1 remains closed long enough, C will fully charge to Ea. You should remember from NEETS, Module 2, Alternating Current and Transformers, that a capacitor takes 5 time constants (5TC) to fully charge.

As the capacitor charges to the applied voltage, the rate of charge follows an exponential curve. If a linear voltage is desired, the full charge time of the capacitor cannot be used because the exponential curve becomes nonlinear during the first time constant.
5.3 Unijunction Sawtooth Generator.

When the 20 volts is applied across B2 and B1, the n-type bar acts as a voltage-divider. A voltage of 12.8 volts appears at a point near the emitter. At the first instant, C1 has no voltage across it, so the output of the circuit, which is taken across the capacitor (C1), is equal to 0 volts. (The voltage across C1 is also the voltage that is applied to the emitter of the unijunction.)

The unijunction is now reverse biased. After T0, C1 begins to charge toward 20 volts. At T1, the voltage across the capacitor (the voltage on the emitter) has reached approximately 12.8 volts. This is the peak point for the unijunction, and it now becomes forward biased.

With the emitter forward biased, the impedance between the emitter and B1 is just a few ohms. This is similar to placing a short across the capacitor. The capacitor discharges very rapidly through the low resistance of B1 to E.

As C1 discharges, the voltage from the emitter to B1 also decreases. Q1 will continue to be forward biased as long as the voltage across C1 is larger than the valley point of the unijunction. At T2 the 3-volt valley point of the unijunction has been reached. The emitter now becomes reverse
biased and the impedance from the emitter to B1 returns to a high value. Immediately after T2, Q1 is reverse biased and the capacitor has a charge of approximately 3 volts. C1 now starts to charge toward 20 volts as it did originally.

The circuit operation from now on is just a continuous repetition of the actions between T2 and T4. The capacitor charges until the emitter becomes forward biased, the unijunction conducts and C1 discharges, and Q1 becomes reverse biased and C1 again starts charging.

Now, let's determine the linearity, electrical length, and amplitude of the output waveform. First, the linearity: To charge the circuit to the full 20 volts will take 5 time constants. In the circuit shown in figure 3-44, view (B), C1 is allowed to charge from T2 to T3. To find the percentage of charge, use the equation:

\[
\text{percent of charge} = \left(\frac{E_{\text{peak}} - E_{\text{valley}}}{E_a - E_{\text{valley}}}\right) \times 100
\]

\[
= \left(\frac{12.8 - 3}{20.0 - 3}\right) \times 100
\]

\[
= \left(\frac{9.9}{17}\right) \times 100
\]

\[
= 57 \text{ percent}
\]

This works out to be about 57 percent and is far beyond the 10 percent required for a linear sweep voltage.

5.4 UJT Relaxation Oscillator

The relaxation oscillator shown in figure consists of UJT and a capacitor C which is charged through resistor \( R_E \) when inter base voltage \( V_{BB} \) is switched on. During the charging period, the voltage across the capacitor increases exponentially until it attains the peak point voltage \( V_p \).

When the capacitor voltage attains voltage \( V_p \), the UJT switches on and the capacitor C rapidly discharges through B1. The resulting current through the external resistor R develops a voltage spike, as illustrated in figure and the capacitor voltage drops to the value \( V_V \).

The device then cuts off and the capacitor commences charging again. The cycle is repeated.
continually generating a saw-tooth waveform across capacitor C. The resulting waveforms of capacitor voltage \( V_C \) and the voltage across resistor \( R \) (\( V_R \)) are shown in figure. The frequency of the input saw-tooth wave can be varied by varying the value of resistor \( R_E \) as it controls the time constant \( (T = R_E C) \) of the capacitor charging circuit.

The discharge time \( t_2 \) is difficult to calculate because the UJT is in its negative resistance region and its resistance is continually changing. However, \( t_2 \) is normally very much less than \( t_1 \) and can be neglected for approximation.

For satisfactory operation of the above oscillator the following two conditions for the turn-on and turn-off of the UJT must be met.

\[
R_E < V_{BB} - V_P / I_P \quad \text{and} \quad R_E > V_{BB} - V_V / I_V
\]

That is the range of resistor \( R_E \) should be as given below

\[
V_{BB} - V_P / I_P > R_E > V_{BB} - V_V / I_V
\]

The time period and, therefore, frequency of oscillation can be derived as below. During charging of capacitor, the voltage across the capacitor is given as

\[
V_c = V_{BB}(1-e^{-t/ReC})
\]

where \( ReC \) is the time constant of the capacitor charging circuit and \( t \) is the time from the commencement of the charging. The discharge of the capacitor commences at the end of charging period \( t_1 \) when the voltage across the capacitor \( V_c \) becomes equal to \( V_P \), that is, \( V_{BB} + V_B \)

\[
V_P = V_{BB} + V_B = V_{BB}(1-e^{-t/ReC}) \quad \text{Neglecting} \quad V_B \quad \text{in comparison to} \quad V_{BB} \quad \text{we have}
\]

\[
\square V_{BB} = V_{BB}(1-e^{-1/ReC})
\]

Or \( e^{-t_1/ReC} = 1 - \square \)

So charging time period, \( t_1 = 2.3 \ RE \ C \log_{10} 1/1- \square \)

![Variable Frequency UJT Relaxation Oscillator](image)

Since discharging time duration \( t_2 \) is negligibly small as compared to charging time duration \( t_1 \) so taking time period of the wave, \( T = t_1 \)
Time period of the saw-tooth wave, \( T = 2.3 \, \text{RE} \, C \, \log_{10} \frac{1}{1-\square} \) and frequency of oscillation \( f = \frac{1}{T} = \frac{1}{2.3 \, \text{RE} \, C \, \log_{10} (1-\square)} \)

By including a small resistor in each base circuit, three useful outputs (saw-tooth waves, positive triggers, and negative triggers), as shown in figure, can be obtained. When the UJT fires, the surge of current through \( B_1 \) causes a voltage drop across \( R_1 \) and produces the positive going spikes.

Also at the UJT firing time, the fall of \( \text{VEB} \) causes \( I_B \) to rise rapidly and generate the negative-going spikes across \( R_2 \), as shown in figure. \( R_1 \) and \( R_2 \) should be much smaller than \( R_{BB} \) to avoid altering the firing voltage of the UJT.

A wide range of oscillation frequencies can be achieved by making \( \text{RE} \) adjustable and including a switch to select different values of capacitance, as illustrated. As already mentioned in previous blog post there is upper and lower limits to the signal source resistance \( \text{RE} \) for the satisfactory operation of the UJT.

5.5 Pulse Transformer

A pulse transformer is a transformer that is optimised for transmitting rectangular electrical pulses (that is, pulses with fast rise and fall times and a relatively constant amplitude). Small versions called signal types are used in digital logic and telecommunications circuits, often for matching logic drivers to transmission lines. Medium-sized power versions are used in power-control circuits such as camera flash controllers. Larger power versions are used in the electrical power distribution industry to interface low-voltage control circuitry to the high-voltage gates of power semiconductors. Special high voltage pulse transformers are also used to generate high power pulses for radar, particle accelerators, or other high energy pulsed power applications.

To minimise distortion of the pulse shape, a pulse transformer needs to have low values of leakage inductance and distributed capacitance, and a high-open-circuit inductance. In power-type pulse transformers, a low coupling capacitance (between the primary and secondary) is important to protect the circuitry on the primary side from high-powered transients created by the load.

For the same reason, high insulation resistance and high breakdown voltage are required. A good transient response is necessary to maintain the rectangular pulse shape at the secondary, because a pulse with slow edges would create switching losses in the power semiconductors.

The product of the peak pulse voltage and the duration of the pulse (or more accurately, the voltage-time integral) is often used to characterise pulse transformers. Generally speaking, the larger this product, the larger and more expensive the transformer.

Pulse transformers by definition have a duty cycle of less than 0.5, whatever energy stored in the coil during the pulse must be "dumped" out before the pulse is fired again.

5.6 Blocking Oscillator

The BLOCKING OSCILLATOR is a special type of wave generator used to produce a narrow pulse, or trigger. Blocking oscillators have many uses, most of which are concerned with the timing of some other circuit. They can be used as frequency dividers or counter circuits and for switching other circuits on and off at specific times.

In a blocking oscillator the pulse width (pw), pulse repetition time (prt), and pulse repetition rate (prr) are all controlled by the size of certain capacitors and resistors and by the operating
characteristics of the transformer. The transformer primary determines the duration and shape of the output. Because of their importance in the circuit, transformer action and series RL circuits will be discussed briefly. You may want to review transformer action in NEETS, Module 2, Introduction to Alternating Current and Transformers before going to the next section.

**Transformer Action**

Figure (A), shows a transformer with resistance in both the primary and secondary circuits. If S1 is closed, current will flow through R1 and L1. As the current increases in L1, it induces a voltage into L2 and causes current flow through R2. The voltage induced into L2 depends on the ratio of turns between L1 and L2 as well as the current flow through L1.

![Diagram of a transformer circuit](image)

**Blocking Oscillator Applications**

A basic principle of inductance is that if the increase of current through a coil is linear; that is, the rate of current increase is constant with respect to time, then the induced voltage will be constant. This is true in both the primary and secondary of a transformer. Figure 3-32, view (B), shows the voltage waveform across the coil when the current through it increases at a constant rate.

Notice that this waveform is similar in shape to the trigger pulse shown earlier in figure 3-1, view (E). By definition, a blocking oscillator is a special type of oscillator which uses inductive regenerative feedback. The output duration and frequency of such pulses are determined by the characteristics of a transformer and its relationship to the circuit.

![Diagram of a blocking oscillator](image)
When power is applied to the circuit, R1 provides forward bias and transistor Q1 conducts. Current flow through Q1 and the primary of T1 induces a voltage in L2. The phasing dots on the transformer indicate a 180-degree phase shift. As the bottom side of L1 is going negative, the bottom side of L2 is going positive. The positive voltage of L2 is coupled to the base of the transistor through C1, and Q1 conducts more.

This provides more collector current and more current through L1. This action is regenerative feedback. Very rapidly, sufficient voltage is applied to saturate the base of Q1. Once the base becomes saturated, it loses control over collector current. The circuit now can be compared to a small resistor (Q1) in series with a relatively large inductor (L1), or a series RL circuit.

![Collector Waveform](image)

### Blocking oscillator idealized waveforms.

The operation of the circuit to this point has generated a very steep leading edge for the output pulse. Figure 3-34 shows the idealized collector and base waveforms. Once the base of Q1 becomes saturated, the current increase in L1 is determined by the time constant of L1 and the total series resistance. From T0 to T1 in figure 3-34 the current increase (not shown) is approximately linear.

The voltage across L1 will be a constant value as long as the current increase through L1 is linear.

At time T1, L1 saturates. At this time, there is no further change in magnetic flux and no coupling from L1 to L2. C1, which has charged during time TO to T1, will now discharge through R1 and cut off Q1. This causes collector current to stop, and the voltage across L1 returns to 0.

The length of time between T0 and T1 (and T2 to T3 in the next cycle) is the pulse width, which depends mainly on the characteristics of the transformer and the point at which the transformer saturates. A transformer is chosen that will saturate at about 10 percent of the total circuit current.

This ensures that the current increase is nearly linear. The transformer controls the pulse width because it controls the slope of collector current increase between points T0 and T1. Since $\text{TC} = \frac{L}{R}$, the greater the L, the longer the TC. The longer the time constant, the slower the rate of current increase. When the rate of current increase is slow, the voltage across L1 is constant for a longer time. This primarily determines the pulse width.
From T1 to T2 (figure 3-34), transistor Q1 is held at cutoff by C1 discharging through R1 (figure3-33). The transistor is now said to be "blocked." As C1 gradually loses its charge, the voltage on the base of Q1 returns to a forward-bias condition. At T2, the voltage on the base has become sufficiently positive to forward bias Q1, and the cycle is repeated.

The collector waveform may have an INDUCTIVE OVERSHOOT (PARASITIC OSCILLATIONS) at the end of the pulse. When Q1 cuts off, current through L1 ceases, and the magnetic field collapses, inducing a positive voltage at the collector of Q1. These oscillations are not desirable, so some means must be employed to reduce them. The transformer primary may be designed to have a high dc resistance resulting in a low Q; this resistance will decrease the amplitude of the oscillations. However, more damping may be necessary than such a low-Q transformer primary alone can achieve.

If so, a DAMPING resistor can be placed in parallel with L1. When an external resistance is placed across a tank, the formula for the Q of the tank circuit is \( Q = \frac{R}{X_L} \), where R is the equivalent total circuit resistance in parallel with L, the Q is directly proportional to the damping resistance (R). In figure 3-35, damping resistor R2 is used to adjust the Q which reduces the amplitude of overshoot parasitic oscillations.

As R2 is varied from infinity toward zero, the decreasing resistance will load the transformer to the point that pulse amplitude, pulse width, and prf are affected. If reduced enough, the oscillator will cease to function. By varying R2, varying degrees of damping can be achieved.

The blocking oscillator discussed is a free-running circuit. For a fixed prf, some means of stabilizing the frequency is needed. One method is to apply external synchronization triggers (figure 3-37), view (A) and view (B). Coupling capacitor C2 feeds input synchronization (sync) triggers to the base of Q1.

If the trigger frequency is made slightly higher than the free-running frequency, the blocking oscillator will "lock in" at the higher frequency. For instance, assume the free-running frequency of this blocking oscillator is 2 kilohertz, with a prf of 500 microseconds. If sync pulses with a prf of 400 microseconds, or 2.5 kilohertz, are applied to the base, the blocking oscillator will "lock in" and run at 2.5 kilohertz. If the sync prf is too high, however, frequency division will occur. This means that if the sync prf is too short, some of the triggers occur when the base is far below cutoff. The blocking
oscillator may then synchronize with every second or third sync pulse. For example, in figure 3-37, view (A) and view (B) if trigger pulses are applied every 200 microseconds (5 kilohertz), the trigger that appears at T1 is not of sufficient amplitude to overcome the cutoff bias and turn on Q1. At T2, capacitor C1 has nearly discharged and the trigger causes Q1 to conduct. Note that with a 200-microsecond input trigger, the output prt is 400 microseconds. The output frequency is one-half the input trigger frequency and the blocking oscillator becomes a frequency divider.
UNIT I

FEEDBACK AMPLIFIERS

1. **State the nyquist criterion to maintain the stability of negative feedback amplifier**
   The nyquist criterion forms the basis of a steady state method of determining whether an amplifier is stable or not.
   **Nyquist Criterion**
   The $A\beta$ is a function of frequency. Points in the complex plane are obtained for the values of $A\beta$ corresponding to all values of ‘f’ from $-\infty$ to $\infty$. The locus of all these points forms a closed curve. The criterion of nyquist is that amplifier is unstable if this curve encloses the point (-1+j0), and the amplifier is stable if the curve does not enclose this point.

![FIG. locus of |1+Aβ|=1](image)

2. **Define sensitivity and desensitivity of gain in feedback amplifiers.**
   **Sensitivity:** The fractional change in amplification with feedback divided by the fractional change in amplification without feedback is called the sensitivity of the transfer gain.
   
   
   $$
   \text{sensitivity} = \left| \frac{A_f}{A} \right| = \frac{1}{1 + A\beta}
   $$

   **Desensitivity:** Desensitivity is defined as the reciprocal of sensitivity. It indicates the factor by which the voltage gain has been reduced due to feedback network.
   
   Desensitivity factor $(D) = 1+A \beta$.

   Where $A = $ Amplifier gain.
   
   $\beta = $ Feedback factor.

3. **What is the effect on input and output impedance of an amplifier if it employs voltage series negative feedback?**
   When voltage series feedback is employed in an amplifier, its input resistance increases and output resistance decreases.

4. **Define ‘feedback factor’ of a feedback amplifier.**
   It is the ratio between the feedback voltages to the output voltage of the amplifier.
   
   $$
   \beta = \frac{V_f}{V_o}
   $$

   Where $\beta$ is a feedback factor (or) feedback ratio. $V_f$ is the feedback voltage. $V_o$ is the output voltage.
5. **What is the impact of negative feedback on noise in circuits?**

When negative feedback is employed in an amplifier, the noise is reduced.

Let \( N \) = noise without feedback

\( N_f = \) noise with feedback

The noise with feedback is given by the following relation

\[
N_f = \frac{N}{1 + A\beta}
\]

From above equation it is clear that when the feedback is applied the noise is reduced by a factor \((1 + A\beta)\)

6. **What is the effect on input and output impedance of an amplifier if it employs current shunt negative feedback?**

When current shunt feedback is employed in an amplifier, its input resistance decreases and output resistance increases.

7. **What is return ratio of feedback amplifier?**

A path of a signal from input terminals through basic amplifier, through the feedback network and back to the input terminals forms a loop. The gain of this loop is the product of \(-A\beta\). This gain is known as loop gain or return ratio. Here the minus sign indicates the negative feedback.

8. **Justify that negative feedback amplifier increases bandwidth.**

When negative feedback is employed in an amplifier, the bandwidth is increased.

Let \( BW \) = bandwidth without feedback

\( BW_f = \) bandwidth with feedback

The bandwidth with feedback is given by the following relation,

\[
BW_f = BW(1 + A\beta)
\]

From above equation it is clear that when the feedback is applied the bandwidth is increased by a factor \((1 + A\beta)\)

9. **Distinguish between series and shunt feedback amplifiers**

**Series feedback:**

(i). In series feedback amplifier the feedback signal is connected in series with the input signal.

(ii). It increases the input resistance.

**Shunt feedback:**

(i). In shunt feedback amplifier the feedback signal is connected in shunt with the input signal.

(ii). It decreases the input resistance.

10. **What is current-series feedback amplifier. (or) What is transconductance amplifier?**

In a current series feedback amplifier the sampled signal is a current and the feedback signal (which is fed in series) is a voltage.

\[
G_m = \frac{I_o}{V_i}
\]

Where \( G_m = \) Amplifier gain.

\( I_o = \) Output current.

\( V_i = \) Input voltage.

11. **List the four basic feedback topologies.**

- Current series feedback.
- Current shunt feedback.
- Voltage series feedback
- Voltage shunt feedback

12. **List the characteristics of an amplifier which are modified by negative feedback.**

- It reduces the gain of an amplifier
- It increases the stability of an amplifier.
- It increases the bandwidth
- It decreases noise and distortion

13. What is Feedback Amplifier? & draw the diagram.
An amplifier with feedback network is known as a feedback amplifier. With the help of feedback network, ‘a portion of the output signal is fed back to the input & combined with the input signal to produce the desired outputs’

14. Mention the three networks that are connected around the basic amplifier to implement the feedback concept.[NOV/DEC 2012]
The three networks that are connected around the basic amplifier to implement the feedback concept are
- Mixing Network
- Sampling Network
- Feedback Network

15. What happens to the input resistance based on the type of feedback in an amplifier?[MAY/JUNE 2009]
- If the feedback signal is added to the input in series with the applied voltage, it increases the input resistance.
- If the feedback signal is added to the input in shunt with the applied voltage, it decreases the input resistance.

16. What are the steps to be carried out for complete analysis of a feedback amplifier?[MAY/JUNE 2009]
Step 1 : Identify the topology
Step 2,3: Find input and output circuit
Step 4 : Replace transistor by its h-parameter equivalent circuit
Step 5 : Find open loop voltage gain
Step 6 : Indicate $V_0$ and $V_f$ and calculate $\beta$
Step 7 : Calculate $D$, $A_{vf}$, $R_{df}$, $R_{of}$ and $R_{of}'$
UNIT II

OSCILLATORS


   The conditions for oscillator to produce oscillation are given by Barkhausan criterion. They are:
   i) The total phase shift produced by the circuit should be 360° or 0°
   ii) The Magnitude of loop gain must be greater than or equal to 1 (ie)|Aβ| ≥ 1

2. What is the major disadvantage of a Twin-T oscillator? [NOV/DEC 2012]
   Twin –T oscillator is operated only at one frequency.

3. Differentiate oscillator from amplifier.[NOV/DEC 2013]

<table>
<thead>
<tr>
<th>Oscillators</th>
<th>Amplifiers</th>
</tr>
</thead>
<tbody>
<tr>
<td>1. They are self-generating circuits. They generate waveforms like sine, square and triangular waveforms of their own. Without having input signal.</td>
<td>1. They are not self-generating circuits. They need a signal at the input and they just increase the level of the input waveform.</td>
</tr>
<tr>
<td>2. It have infinite gain</td>
<td>2. It have finite gain</td>
</tr>
<tr>
<td>3. Oscillator uses positive feedback.</td>
<td>3. Amplifier uses negative feedback.</td>
</tr>
</tbody>
</table>

4. State Barkhausen criterion for sustained oscillation. What will happen to the oscillation if the magnitude of the loop gain is greater than unity?[NOV/DEC 2013]

   The conditions for oscillator to produce oscillation are given by Barkhausan criterion. They are:
   i) The total phase shift produced by the circuit should be 360° or 0°
   ii) The Magnitude of loop gain must be greater than or equal to 1 (ie)|Aβ| ≥ 1
   In practice loop gain is kept slightly greater than unity to ensure that oscillator work even if there is a slight change in the circuit parameters.

5. Why an LC tank circuit does not produce sustained oscillations. How can this can be overcome?[NOV/DEC 2008]

   We know that the inductor coil has some resistance and dielectric material of the capacitor has some leakage.so small part of the originally imparted energy is used to overcome these losses. As a result, the amplitude of oscillating current goes on decreasing and becomes zero when all energy is consumed as losses. So a LC tank circuit does not produce sustained oscillations.
   To maintain sustained oscillations, energy must be supplied to the circuit at the same rate at which it is dissipated. In an oscillator, the function of transistor and power supply source is to feed energy to the circuit to overcome the losses at right time.

The crystal actually behaves as a series RLC circuit in parallel with $C_M$. Because of the presence of $C_M$, the crystal has two resonant frequencies.

- One of these is the series resonant frequency $f_s$. In this case impedance is very low.

$$f_s = \frac{1}{2\pi \sqrt{LC}}$$

- The other is parallel resonance frequency $f_p$. In this case impedance is very high.

$$f_p = \frac{1}{2\pi \sqrt{LC_{eq}}}, \text{where } C_{eq} = \frac{C C_M}{C + C_M}$$

7. **What are the advantages and disadvantages of RC phase shift oscillators?** [APR/MAY 2008]

**Advantages:**

i. It is best suited for generating fixed frequency signals in the audio frequency range.

ii. It requires no transformer or inductor, hence less bulky.

iii. Simple Circuit.

*Pure sine wave output is possible.

**Disadvantages:**

i) It requires a high $\beta$ transistor to overcome losses in the network.

ii) These oscillators are not suitable for high frequency operation.

iii) Frequency of oscillation cannot be changed easily. To change the frequency of oscillation, the three capacitor or resistors should be changed simultaneously. This is inconvenient.

8. **What is the necessary condition for a Wien bridge oscillator circuit to have sustained oscillations?** [MAY/JUNE 2013]

Then for oscillations to occur in a **Wien Bridge Oscillator** circuit the following conditions must apply.

- With no input signal the Wien Bridge Oscillator produces output oscillations.

- The Wien Bridge Oscillator can produce a large range of frequencies.

- The Voltage gain of the amplifier must be at least 3.

- The network can be used with a Non-inverting amplifier.

- The input resistance of the amplifier must be high compared to R so that the RC network is not overloaded and alter the required conditions.

- The output resistance of the amplifier must be low so that the effect of external loading is minimised.

9. **Define piezoelectric effect.** [MAY/JUNE 2006]

The piezoelectric Crystals exhibit a property that if a mechanical stress is applied across one face the electric potential is developed across opposite face and vice versa. This phenomenon is called piezo electric effect.
10. What is the principle behind operation of a crystal oscillator?[NOV/DEC 2007]
The principle behind the operation of crystal is piezoelectric effect. According to this effect, if a
tmechanical stress is applied across one face the electric potential is developed across opposite face
and vice versa.

11. Draw an oscillator circuit with feedback network given below.[MAY/JUNE 2006]

12. What are the advantages and disadvantages of wein bridge oscillators?

**Advantages:**
1. Provides a stable low distortion sinusoidal output over a wide range of frequency.
2. The frequency range can be selected simply by using decade resistance boxes.
3. The frequency of oscillation can be easily varied by varying capacitances $C_1$ and $C_2$
simultaneously. The overall gain is high because of two transistors.

**Disadvantages:**
1. The circuit needs two transistors and a large number of other components.
2. The maximum frequency output is limited because of amplitude and the phase-shift characteristics
   of amplifier.

13. A weinbridge oscillator is used for operations at 9KHz. If the value of resistance $R$ is 100KΩ,
what is the value of $C$ required?[APRIL/MAY 2011]

14. A weinbridge oscillator is used for operations at 10KHz. If the value of resistance $R$ is
100KΩ, what is the value of $C$ required?[NOV/DEC 2008]
15. A tuned collector oscillator in a radio receiver has a fixed inductance of 60µH and has to be tunable over the frequency band of 400KHz to 1200KHz. Find the range of variable capacitor to be used.[APRIL/MAY 2011, NOV/DEC 2011]

16. Draw the feedback circuit of a colpitts oscillator. Obtain the value of the equivalent series capacitance required if it uses a L of 100mH and is to oscillate at 40KHz.[MAY/JUNE 2013]

17. In a Hartley oscillator if L1=0.2mH, L2=0.3mH and C=0.003µF. calculate the frequency of its oscillations.[MAY/JUNE 2012, NOV/DEC 2012]

18. In an RC phase shift oscillator, if its frequency of oscillation is 955Hz and R1=R2=R3=680KΩ. Find the value of capacitors.[NOV/DEC 2010]

19. In an RC phase shift oscillator, if R1=R2=R3=200KΩ and C1=C2=C3=100pF. Find the frequency of the oscillator.[APR/MAY 2010]

20. A crystal has the following parameters L=0.5H, C=0.05pF and mounting capacitance is 2pF. Calculate its series and parallel resonating frequencies.[NOV/DEC 2010]

21. Calculate the frequency of oscillation for the clap oscillator with C1=0.1µF, C2=1µF, C3=100pF and L=470µH.[MAY/JUNE 2007]
UNIT III TUNED AMPLIFIERS

1. **What is tuned amplifier? What are the various types of tuned amplifiers? [NOV/DEC 2013]**
   A tuned amplifier amplifies a certain range of frequencies (narrow band of frequencies) in the radio frequency region and rejects all other frequencies.
   
   **Types:**
   The various types of tuned amplifiers are
   i) Single tuned amplifier
   ii) Double tuned amplifier
   iii) Stagger tuned amplifier & synchronously tuned amplifier.

2. **Define tuned amplifier. [APRIL/MAY 2010]**
   A tuned amplifier is defined as an amplifier circuit which amplifies a certain range of frequencies (narrow band of frequencies) in the radio frequency region and reject all other frequencies.

3. **Why tuned amplifier cannot be used at low frequency?**
   For low frequencies the size L and C are large. So the circuit will be bulky and expensive, hence the tuned amplifiers cannot be used at low frequency.

4. **What is the other name for tuned amplifier?**
   Tuned amplifiers used for amplifying narrow band of frequencies hence it is also known as “narrow band amplifier” or “Band pass amplifier”.

5. **Mention The Two Applications of tuned amplifiers. [NOV/DEC 2007, NOV/DEC 2008]**
   i) They are used in IF amplifiers in Radio and TV receivers.
   ii) They are used in wireless communication systems.

6. **State two advantages and two disadvantages of tuned amplifiers. [MAY/JUNE 2012]**
   **Advantages:**
   i) They amplify defined frequencies
   ii) Signal to noise ratio (SNR) at output is good.
   iii) They are suited for radio transmitters and receivers.
   
   **Disadvantages:**
   i) They are not suitable to amplify audio frequencies.
   ii) Circuit is bulky and costly.
   iii) The design is complex.

7. **What is Single tuned and double tuned amplifier?**
   **Single tuned amplifier:**
   An amplifier circuit that uses a single parallel tuned circuit as a load is called single tuned amplifier.
   
   **Double tuned amplifier:**
   The amplifiers having two parallel resonant circuit in its load are called double tuned amplifiers.

8. **What are the advantages of double tuned amplifier over single tuned amplifier?**
   i) Provides higher gain
   ii) Provides large 3dB bandwidth.
   iii) Possess flatter response having steeper sides.
9. What are the different coil losses?
i) Hysteresis loss
ii) Copper loss
iii) Eddy current loss

10. What are the differences between single tuned and synchronously tuned amplifiers?[NOV/DEC 2007]

<table>
<thead>
<tr>
<th>Single tuned amplifier</th>
<th>Synchronously tuned amplifier</th>
</tr>
</thead>
<tbody>
<tr>
<td>• Uses one parallel tuned circuit as the load impedance and tuned to one frequency.</td>
<td>• Uses a number of identical cascaded single tuned stages tuned to same frequency.</td>
</tr>
<tr>
<td>• High gain and narrow bandwidth</td>
<td>• Increases gain and reduces bandwidth.</td>
</tr>
<tr>
<td>• Bandwidth is [ BW = \frac{f_c}{Q} ]</td>
<td>• The bandwidth equation is [ BW_n = BW_1 \sqrt{2^{1/n} - 1} ]</td>
</tr>
</tbody>
</table>

11. What is Stagger tuned amplifier?[NOV/DEC 2011]
If two or more tuned circuits which are cascaded are tuned to slightly different resonant frequencies, it is possible to obtain an increased bandwidth with a flat passband with steep sides. This technique is known as stagger tuning and the amplifier using this technique is called as stagger tuned amplifier.

12. What are the different types of neutralization?
i) Hazeltine neutralization
ii) Neutrodyne neutralization
iii) Rice neutralization

In order to prevent oscillations in tuned RF amplifiers it was necessary to reduce the stage gain to a level that ensured circuit stability. This can be accomplished in several ways such as lowering the Q of the tuned circuits, stagger tuning, loose coupling between the stages. Instead of losing the circuit performance to achieve stability, a circuit in which the troublesome effect of the collector to base capacitance of the transistor was neutralised by introducing a signal which cancels the signal coupled through the collector to base capacitance.

**Unloaded Q:**
It is defined as the ratio of stored energy to dissipated energy in a reactor or resonator.
For an inductor or capacitor

\[ Q_u = \frac{X}{R_s} \]

Where \( X \) = reactance; \( R_s \) = series resistance

**Loaded Q:**
The loaded Q or \( Q_L \) of a resonator is determined by how tightly the resonator is coupled to its terminations.

\[ Q_L = 2\pi \times \frac{\text{Maximum energy stored per cycle}}{\text{Energy dissipated per cycle} + \text{Energy dissipated due to external load}} \]

15. What is the effect of cascading n stages of identical single tuned amplifiers (synchronously tuned) on the overall 3dB bandwidth? [APRIL/MAY 2011]
The bandwidth of n stage cascaded single tuned amplifier is given as

\[ BW_n = BW_1 \sqrt{\frac{2^{1/n} - 1}{n}} \]

From the above equation it is clear that the overall 3dB bandwidth reduces.

16. Mention the bandwidth of a double tuned amplifier

\[ \text{Bandwidth}(\omega_2 - \omega_1) = \frac{\omega_c}{Q} \sqrt{(b^2 - 1) + 2b} \]

Where \( \omega_c \) is the resonance frequency in cycle/sec
\( Q \) is the Quality factor of the coil alone
\( b \) is a constant

17. Where is the Q-point placed in a class C type amplifier? What are its applications? [APR/MAY 2008]
In a class C type amplifier the Q-point is placed below the X-axis.

**Applications:**
18. Brief the relation between bandwidth and Q-factor. [MAY/JUNE 2007]
The quality factor determines the 3dB bandwidth for the resonant circuit. The 3dB bandwidth for resonant circuit is given by
\[ BW = \frac{f_r}{Q} \]
Where \( f_r \) = centre frequency of a resonator
\( BW = f_2 - f_1 \)
If Q is large bandwidth is small.
If Q is small bandwidth is large.

The process of cancelling the instability effect due to the collector to base capacitance of the transistor in tuned circuits by introducing a signal which cancels the signal coupled through the collector to base capacitance is called narrow band neutralization.

20. Mention two important features of stagger tuned amplifier. [MAY/JUNE 2013]
i) It has better flat, wide band characteristics.
ii) Increased bandwidth

21. What is the need for neutralization circuits? [MAY/JUNE 2013, NOV/DEC 2008]
In tuned RF amplifiers, the inter-junction capacitance \( C_{bc} \) of the transistor becomes dominant (i.e) its reactance is low, it provides the feedback signal from collector to base. If some feedback signal manages to reach the input from output in a positive manner with proper phase shift, then amplifier keeps oscillating, thus stability of amplifier gets affected. Hence neutralization is employed.

22. Draw a class C tuned amplifier circuit and what is its efficiency. [MAY/JUNE 2006]
\[ \eta = \frac{P_{out}}{P_2} \times 100\% \]
At conduction angle \( \theta = 180^\circ \), \( \eta = 78.5\% \)

23. Derive the resonance frequency for the tank circuit shown: [NOV/DEC 2006]
At resonance \( X_L = X_C \)
\[ 2\pi f_r L = \frac{1}{2\pi f_r C} \]
Resonance frequency \( f_r = \frac{1}{2\pi \sqrt{LC}} \)

24. A tuned circuit has resonant frequency of 1600 KHz and bandwidth of 10 KHz. What is the value of its Q-factor? [MAY/JUNE 2012]

25. A tuned amplifier has its maximum gain at a frequency of 2 MHz and has a bandwidth of 50 KHz. Calculate the Q-factor. [NOV/DEC 2006]
26. An inductor of 250\(\mu\)H has \(Q=300\) at 1MHz. Determine \(R_s\) and \(R_p\) of the inductor.[NOV/DEC 2012,MAY/JUNE 2006]

27. A parallel resonant circuit has an inductance of 150\(\mu\)H and a capacitance of 100pF. Find the resonant frequency.[NOV/DEC 2011,MAY/JUNE 2007]
UNIT IV
WAVE SHAPING CIRCUITS AND MULTIVIBRATORS

1. Give two applications of bistable multivibrators (APRIL/MAY 2010, APRIL/MAY 2011)
   • Used to generate symmetrical square wave. This is possible by using triggering pulses of equal
     interval, corresponding to the frequency required.
   • Used as a memory element in shift registers, counters, etc.,
   • Used for the performance of many digital operations like counting and storing of digital
     information.
   • Can be used as a frequency divider

2. How does a diode act as a comparator? (NOV/DEC 2010)

   A Comparator Circuit is used to identify the instant at which the arbitrary input waveform attains a
   particular reference level. Basically it is a clipper circuit. A simple diode comparator and its
   equivalent circuit is given as

   Consider $V_{in}$ as a ramp input, increasing linearly from zero. The output will remain at $V_R$, till input is
   less than $V_R + V_Y$, as the diode is not conducting. (ie) $V_o = V_R$ for $V_{in} < V_R + V_Y$

   At $t=t_1$, $V_{in}$ becomes equal to $V_R + V_Y$ after which $V_o$ increases along with the input signal $V_{in}$.

   The comparator output is given to a particular device. This device will respond when the
   comparator voltage increases to some level of $V_o$ above $V_R$.

3. What is meant by clipper circuit? (APRIL/MAY 2011)

   The electronic circuits which are used to clip off the unwanted portion of the waveform, without
   distorting the remaining part of the waveform are called clipper circuits.

4. What is the 'tilt' applicable to RC circuits? Give an expression for tilt. (NOV/DEC 2011)

   In high pass RC network, Tilt is defined as the decay in the amplitude of the output
   voltage waveform, when the input maintains its level constant.

   Percentage of tilt is given by

   $$P = \frac{V - V'}{V/2} \times 100$$

   Therefore

   $$P = \frac{T}{2RC} \times 100\%$$

   Where T- time period
5. **What type of distortion is observed in astable multivibrator?** (NOV/DEC 2011)

It can be seen that, in the collector waveforms shown in the figure there is certain distortion present. Instead of [Vc1, Vc2] exact square wave, we are getting the vertical rising edges little bit rounded. This is called **rounding**. For a square wave output such a rounding is undesirable and must be eliminated.

6. **What is meant by clamper circuit?** (MAY/JUNE 2012, NOV/DEC 2009)

The electronic circuits which are used to add a dc level as per the requirement to the ac output signal are called clamper circuits.

It is also known as dc inserter or dc restorer.

7. **Give two applications of Schmitt Trigger circuit.** (MAY/JUNE 2012).

   - It is used as an amplitude comparator
   - It can be used as a squaring circuit.
   - It can be used as a sine wave to square wave converter

8. **Why do we call astable multivibrator as free running multivibrator?** (NOV/DEC 2012)

An astable multivibrator is called free running multivibrator because it generates square waves of its own without any external triggering pulse.

9. **Define the threshold points in a Schmitt trigger circuit.** (NOV/DEC 2013)

   - Schmitt trigger is a type of comparator with two different threshold voltage levels on points (UTP, LTP).
   - Whenever the input signal goes over the high threshold levels, the output of the comparator is switched high. The output will remain in this same state as long as the input voltage is above the low threshold level.
   - When the input voltage goes below this level, the output will switch. These threshold voltage levels are called threshold points.

10. **What is a regenerative comparator? Give example circuit.** (MAY/JUNE 2013)

Regenerative comparator is a circuit, compares its input voltage to a “threshold voltage”, because it has two threshold voltages (the upper and lower trigger voltages). The threshold voltage depends on the output state. If the input voltage is higher than the upper trigger voltage, the output will be high. A small amount of the output voltage is effectively added to the input voltage before it is compared to a fixed threshold. So it uses positive (or) regenerative feedback.

E.g.: Schmitt Trigger

11. **Distinguish between symmetrical and unsymmetrical triggering methods.** [NOV/DEC 2009]

Symmetrical triggering uses only one trigger input and unsymmetrical triggering uses two trigger input.

12. **Why Monostable multivibrator is also called as delay circuit?** [MAY/JUNE 2009]

Used to introduce time delay as gate width is adjustable.

13. **Determine the value of capacitors to be used in an astable multivibrator to provide a train of pulse of 4μs wide at a repetition rate of 80KHz if R1=R2=10K.** (NOV/DEC 2013)

Given
14. A 20 KHz, 75% duty cycle square wave is used to trigger continuously, a monostable multivibrator with triggered pulse duration of 5µs. What will be the duty cycle of the output of the monostable multivibrator? (APRIL/MAY 2010)

15. A RC low pass circuit has R=1.5Kohm and C=0.2micro farad. What is the rise time of the output when excited by a step input.(MAY/JUNE 2013)

16. In a low pass RC circuit, rise time is 35 nano seconds. What is the bandwidth that can be obtained using the circuit?(NOV/DEC 2012)

17. Determine the value of capacitors to be used in an astable multivibrator to provide a train of pulse 2µs wide at a repetition rate of 75KHz with R1=R2=10KHz. (NOV/DEC 2010)
UNIT V

BLOCKING OSCILLATORS AND TIMEBASE GENERATOR


   **Slope error (or) sweep speed error ($e_s$):**
   Slope error is defined as the ratio of the difference in slope at beginning and end sweep to the initial value of the slope. It is also called as sweep speed error ($e_s$)

   \[ e_s = \frac{\text{Difference in slope at beginning and end of sweep}}{\text{Initial value of slope}} \]

   **Displacement Error ($e_d$):**
   It is defined as the maximum difference between the actual sweep voltage and linear sweep which passes through the beginning and end points of the actual sweep.
   The displacement error is given as

   \[ e_d = \frac{(V' - V_s)_{\text{max}}}{V_s} \]


   - Used as a main device to supply triggers for synchronization of a system having pulse type waveforms
   - Used as a Frequency Divider or Counter
   - Used to produce large peak power pulses.
   - As a low impedance switch

3. State any two applications of pulse transformer.(MAY/JUNE 2012)

   - To act as a coupling element in certain pulse generating circuits such as blocking oscillators
   - To invert the polarity of pulse
   - To provide dc isolation between source and a load
   - To produce pulse in a circuit having negligible dc resistance
   - To differentiate a pulse

4. What are 'Restoration time' and 'Sweep time' of a time base signal?(MAY/JUNE 2012)

   **Restoration time ($T_r$):**
   It is the time required for the return to its initial value. It is also called as **return time** or **flyback time**.

   **Sweep time ($T_s$):**
   It is the period during which voltage increases linearly
5. List the applications of time base generators. (NOV/DEC 2013)
   - Used in CRO (Cathode Ray Oscilloscope)
   - Used in Television and radar displays
   - Used in precise time measurements
   - Used in time modulation

6. What are the advantages of core saturation method of frequency control in a blocking oscillator? (NOV/DEC 2012)

   The pulse duration depends on the supply voltage and characteristics of the core and not on the transistor parameters ($h_{fe}$).

   The pulse width is given by

   $$t_p = \frac{(n + 1)NAB_m}{V_{ee}}$$

7. State any two methods of achieving sweep linearity of a time-base waveform. (NOV/DEC 2012)
   - Exponential charging
   - Constant current charging
   - Miller circuit
   - Bootstrap circuit.

8. Draw the equivalent circuit of a pulse transformer. Name the various elements in it. (NOV/DEC 2011, NOV/DEC 2009)

   $R_1$ = Primary winding and source resistance
   $R_2$ = Total resistance reflected to primary side
   $\sigma$ = Leakage inductance
   $L$ = Magnetizing inductance
   $C$ = Total effective shunt capacitance

9. What is the function of time base circuit? (APRIL/MAY 2010)

   A linear time base generator produces an output waveform, which produces a portion which exhibits a linear variation of voltage or current with respect to time.

10. What is blocking oscillator?

    The circuit which uses a regenerative feedback, producing a single pulse or pulse train is called a blocking oscillator.
11. Which are the two important elements of a blocking oscillator?

   1. Active element like transistor.
   2. A pulse transformer.

12. What is the function of pulse transformer in blocking oscillator?

   A pulse transformer is used to couple output of the transistor back to the input. The nature of such feedback through pulse transformer is controlled by relative winding polarities of a pulse transformer.

13. What is pulse transformer?[APR-2004]

   A pulse transformer is basically a transformer which couples a source of pulses of electrical energy to the load, keeping the shape and other properties of pulses unchanged. The voltage level of the pulse can be raised or lowered by designing the proper turns ratio for the pulse transformer.

14. Draw a transistorized bootstrap time base generator circuit?(NOV/DEC 2010)

15. Draw the circuit diagram of astable blocking oscillator. (NOV/DEC 2009)
UNIT 1

FEEDBACK AMPLIFIERS